

NOTICE

THIS DOCUMENT HAS BEEN REPRODUCED
FROM THE BEST COPY FURNISHED US BY
THE SPONSORING AGENCY. ALTHOUGH IT
IS RECOGNIZED THAT CERTAIN PORTIONS
ARE ILLEGIBLE, IT IS BEING RELEASED
IN THE INTEREST OF MAKING AVAILABLE
AS MUCH INFORMATION AS POSSIBLE.

NASA CR-54583
GE R67FPD248

SINGLE STAGE EXPERIMENTAL EVALUATION OF
HIGH MACH NUMBER COMPRESSOR ROTOR BLADING
PART 3 - PERFORMANCE OF ROTOR 2E

by

J. P. Gostelow and K. W. Krabacher

prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

September 29, 1967

CONTRACT NO. NAS3-7617

Technical Management
NASA Lewis Research Center
Cleveland, Ohio
James J. Watt, Project Manager
Everett E. Bailey, Research Advisor

ADVANCED TECHNOLOGY AND DEMONSTRATOR PROGRAMS DEPARTMENT
FLIGHT PROPULSION DIVISION
GENERAL ELECTRIC
LYNN, MASSACHUSETTS/CINCINNATI, OHIO

SINGLE STAGE EXPERIMENTAL EVALUATION OF
HIGH MACH NUMBER COMPRESSOR ROTOR BLADING

PART 3 - PERFORMANCE OF ROTOR 2E

by
J.P. Gostelow and K.W. Krabacher

ABSTRACT

A 1400 foot per second tip speed rotor with a 0.5 hub-tip radius ratio, designed to deliver a total pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec, was tested with an undistorted inlet. For conditions at design speed, judged to have adequate stall margin for engine operation, a total-pressure ratio of 1.711 and an adiabatic efficiency of 0.869 were achieved at a flow of 225.9 lbs/sec. The peak adiabatic efficiency of 0.884 at design speed occurred close to the stall line.

SUMMARY

A 1400 foot per second tip speed rotor, designed to have a diffusion factor of 0.45 at the tip, was tested with an undistorted inlet flow. A new type of blade shape has been employed in which the camberline consists of two circular arcs that are mutually tangent at the point where they join. The tip element was designed to have a camber ratio (ratio of supersonic camber to total camber) of 0.35; this value is intermediate between the extreme cases of a double-circular-arc blade section and a blade section having the minimum supersonic camber which is consistent with flow choking limitations. This type of tip shape was smoothly blended into a double-circular-arc shape at approximately the 60% span location. The hub-tip radius ratio at inlet is 0.50. Neither inlet guide vanes nor a stator vane row were employed.

The rotor was designed to deliver a total-pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec. For conditions on the 100% speed line judged to have adequate stall margin for engine operation a total-pressure ratio of 1.711 and an adiabatic efficiency of 0.869 were achieved at a flow of 225.9 lbs/sec. The peak adiabatic efficiency of 0.884 at design speed occurred close to the stall line.

Blade element data were obtained from measurements over a range of speeds from 50% to 110% design speed. Results of these blade element measurements were used to show the variation of deviation angle, diffusion factor and loss coefficient as a function of incidence angle. The rotor was also stalled at these speeds and overall performance data were obtained, while in stall, up to 100% speed. The stall type was rotating stall at all speeds.

INTRODUCTION

In the previous report (ref. 1) the feasibility of efficiently operating a conventionally loaded medium-aspect-ratio rotor at a tip speed of 1400 feet per second was demonstrated. However, for the potential benefits of transonic compressors to be fully realized, it is desirable for the level of total-pressure-rise obtained in one stage to be even higher than that previously obtained. For this reason it was desired to obtain performance data at a higher loading level corresponding to a design tip diffusion factor of 0.45, which can be compared with the previously used value of 0.35. While the use of a diffusion factor is a great help in the definition of rotor loading, considerations of shock losses in transonic passages clearly have at least as important a contribution to make in assessing blade loading capabilities. The design objective of the three more highly loaded rotors was therefore to determine the performance potential of such rotors and if possible to optimize the rotor blade proportions in such a way that the rotor could be more highly loaded without significant sacrifice in efficiency.

Rotor 2E, the second of a series of four medium-aspect-ratio rotors, is designed for a tip diffusion factor of 0.45. A new type of blade shape has been employed, in which the camberline consists of two circular arcs that are mutually tangent at the point where they join. Similarly the suction and pressure surfaces are also each composed of two circular arcs which are mutually tangent at their junction point. The suction surface junction point is directly across the flow passage from the leading edge of the adjacent blade that forms the other side of the flow passage. The front arc is identified as the supersonic arc, and the rear arc is identified as the subsonic arc. The term, camber ratio, refers to the ratio of the camber of the supersonic arc to the total camber. Blade elements developed in this way are called multiple-circular-arc sections. The Rotor 2E blade was designed to have a camber ratio of 0.35; this value is intermediate between the two extreme cases of a double-circular-arc blade section and a blade section having the minimum supersonic camber which is consistent with flow choking limitations, as used in Rotors 2D and 2B respectively. All rotors have double-circular-arc elements from the hub outboard to approximately the 60% span location.

Details of the design of Rotor 2E and the other rotors to be evaluated in this test series are given in reference 2. This report presents results of tests, on Rotor 2E, with a uniform inlet flow.

SYMBOLS

The following symbols are used in this report:

A flow area, in²

A_j	area represented by each discharge rake element. This is the area of an annulus bounded either by radii midway between those of two adjacent elements or by the hub or casing, in ²
a	distance along chord line to position where maximum perpendicular displacement between camberline and chord line occurs, in
c_h	enthalpy-equivalent static-pressure-rise coefficient,
c_p	static-pressure-rise coefficient, $c_p = \frac{p_2 - p_1}{p'_1 - p_1}$
c	blade chord length, in
c_p	specific heat at constant pressure, Btu/lb-°R
D	diffusion factor,
	$D = 1 - \frac{v'_2}{v'_1} + \frac{r_2 v_{\theta 2} - r_1 v_{\theta 1}}{2 r \sigma v'_1}$
g	acceleration due to gravity, 32.174 ft/sec ²
i	incidence angle, difference between air angle and camber line angle at leading edge in cascade projection, deg
J	mechanical equivalent of heat, 778.161 ft-lb/Btu
M	Mach number
P	total or stagnation pressure, psia
p_{in}	compressor inlet average total pressure, psia
p_j	arithmetic average total pressure at j immersion, psia
p	static or stream pressure, psia
r	radius, in

\bar{r}	mean radius, average of streamline leading-edge and trailing-edge radii, in
T	total or stagnation temperature, °R
T_j	arithmetic average total temperature at j immersion, °R
t	static or stream temperature, °R
t	blade thickness, in
t_e	blade edge thickness, in
t_m	blade maximum thickness, in
U	rotor speed, ft/sec
V	air velocity, ft/sec
V_{zj}	average axial velocity at j immersion, ft/sec
w	weight flow, lb/sec
Z	displacement along compressor axis, in
β	air angle, angle whose tangent is the ratio of tangential to axial velocity, deg
γ	ratio of specific heats
γ°	blade-chord angle, angle in cascade projection between blade chord and axial direction, deg
δ	ratio:- $\frac{\text{total pressure}}{\text{standard pressure}}$, $\frac{\text{psia}}{14.696 \text{ psia}}$
δ°	deviation angle, difference between air angle and camber line angle at trailing edge in cascade projection, deg
ϵ°	meridional angle, angle between tangent to streamline projected on meridional plane and axial direction, deg
θ	ratio: - $\frac{\text{total temperature}}{\text{standard temperature}}$, $\frac{^\circ\text{R}}{518.688^\circ\text{R}}$
θ°	angular displacement about compressor axis, deg
η	efficiency

κ°	angle between cylindrical projection of \vec{i}_K and axial direction, deg
ρ	static or stream density, $\text{lb-sec}^2/\text{ft}^4$
ϕ°	camber angle, difference between angles, in cascade projection, of tangents to camber line at extremes of camber line arc, deg
σ	solidity, ratio of chord to spacing
ψ	stream function; $\psi_h = 0$, $\psi_c = 1$
$\bar{\omega}$	total-pressure-loss coefficient
Subscripts:	
a	point on camber line where maximum camber line rise occurs
ad	adiabatic
an	annulus value
c	tip or casing at any plane
d	downstream
e	equivalent two-dimensional cascade
h	hub at any plane
m	meridional direction
p	polytropic
s	suction surface
t	tip at rotor leading edge plane
t	total when referring to blade element
u	upstream
z	with respect to axial displacement
θ	with respect to meridional displacement
1	leading edge
2	trailing edge
0.05, 0.86, 0.95, 1.51, 1.57, 2.0	instrumentation plane designations (fig. 5)

Superscripts:

* critical flow condition

' relative to rotor

APPARATUS AND PROCEDURE

Test Rotor

The design of the rotor used in this test investigation is presented in reference 2 in which it is identified as Rotor 2E. The rotor was designed for a corrected weight flow per unit frontal area of 29.66 lbs/sec per square foot. With the selected rotor tip diameter of 36.5 inches and the hub-tip radius ratio of 0.50, the design corrected weight flow is 215.49 lbs/sec. The selection of a rotor tip solidity of 1.3, a diffusion factor of 0.45, zero inlet swirl, a rotor tip speed of 1400 ft/sec, and an axial velocity ratio of 0.91 permitted the calculation of the change in angular momentum across the rotor at the rotor tip. This change in angular momentum, with a suitable rotor total-pressure-loss coefficient derived from the NASA method of references 3 and 4, resulted in a design rotor total-pressure ratio of 1.76. The design total-pressure ratio was held constant radially. Because the loss correlation resulted in radially varying losses, a radial variation of the change in angular momentum was used in the design vector diagram calculations.

Double-circular-arc blade sections were used in the cascade projection* along the radial height of the blade between the hub and a point approximately 60 per cent of the span away from the hub. Multiple-circular-arc sections were used in the remaining portion of the blade. Blade design data appear in Table 1. An overall view of the assembled Rotor 2E appears in figure 1(a) and a close-up view of the tip section is shown in figure 1(b).

In order to assess the quality of the blading after manufacture, the blading was inspected by means of contour layouts from six of the twelve manufacturing sections for seven blades selected at random from the batch. A meridional view of the rotor appears in figure 2 and the inspected sections are identified by asterisks. At each manufacturing section the average of the seven blades was obtained and was compared with the design intent. The results of the comparisons of the average blade sections with design intent appear in figures 3(a) through 3(f). These figures show the blade

*As described in reference 2, the cascade projection is obtained by viewing the intersection of a blade and an axisymmetric stream surface in the radial direction. The justification for the use of this projection is given in reference 5.

as measured in its cold (zero speed) condition. At first sight the agreement between measured and design sections does not appear to be good, the error being equivalent to a stagger change in which the measured sections are more closed than design intent. However, a small manufacturing discrepancy was also present in the part-span shrouds which enabled the blade to open up more than design intent as the rotor was accelerated to design speed. These errors partially compensated each other and the maximum errors remaining at design speed were such that the blade was about 0.2° more open than design intent at sections outboard of the shroud and about 0.3° more closed than design intent at sections between the shroud and the hub.

The average running tip clearance at 100% speed was 0.043 inches.

Test Facility and Instrumentation

Performance tests of this rotor were made in General Electric's House Compressor Test Facility, at Lynn, Massachusetts. A diagram of the test set up is given in figure 4 and the facility is described in reference 1. Instrumentation was also identical with that used for the testing of Rotor 1B, with the exception of the rotor exit total temperature and total pressure rakes, which had elements at the five new radial positions corresponding to the 10%, 30%, 50%, 70% and 90% immersions. The meridional and circumferential locations of instrumentation are shown in figures 5 and 6 respectively. The general construction features of the fixed rakes and traverse probes are illustrated in figures 7 and 8.

General Test Procedure

The following test sequence was followed, in general, during the testing of this rotor. With the throttle valve set to deliver approximately the design total-pressure ratio at 100% corrected speed, data were recorded from fixed instrumentation at 50%, 70%, 90%, 100% and 110% corrected speeds. (When only fixed-instrumentation measurements are taken, the data readings are termed green readings). The test rotor was returned to 50% corrected speed and the throttle valve closed until the limit of stall-free operation was achieved. With the throttle re-set so that the vehicle operated as close to stall as feasible, blade element data and a green reading were obtained at each speed over the remaining portion of stall-free operation up to the maximum facility flow capacity. Green readings and hot-wire data were then obtained in the stall region with the throttle valve closed to the setting where stall-free operation terminated. All data points are listed in table 2.

Because of the small pressure rise at the 50% and 70% speeds, accurate performance measurements were not obtained from absolute pressure readings. Therefore these two speed lines were re-run with the instrumentation hook-up revised to provide measurements of pressure rise across the rotor rather than absolute pressures. The readings for which the results are presented

on this basis are identified in table 2.

Testing in the Unstalled Region

For all speeds the throttle positions at which data were recorded in the stall free region of operation were generally selected to give the closest spacing of the points on the map at those places where curvature of the speed line was greatest. At low speeds, this led to a relatively even spacing whereas, at higher speeds, the throttle positions were concentrated in the higher pressure ratio region where incidence variations occur.

At the rotor inlet traverse location, the static pressure wedge was set to zero flow direction and the cobra probe was allowed to seek its nulled position. At the rotor exit traverse location the static pressure wedge was manually rotated to the angle orientation established by the nulled position of the cobra probe; since stationary vane rows and struts were relatively far removed from this plane, circumferential variations of angle were presumed to be sufficiently small not to affect the pressure read by the wedge static probe. Probe immersion indicators and the probe aerodynamic parameters were connected to conventional X-Y plotting equipment. Continuous traverses were only recorded for the rotor exit flow angle; these were used to give an indication of the radial extent of the part-span shroud wake. Recording of data from the traversing probes at the standard immersions was achieved by means of a digitized read-out on punched paper tape, as was also the case for the recording of data from fixed instrumentation.

Stall Testing

Upon closing the throttle valve, rotating stalls were encountered, at all speeds. The rotor was stalled twice at each speed, the limit of stall free operation being established by closing the throttle valve slowly until performance and stress changes were noted. For the first stall at each speed the three traverse hot-wire anemometer probes were immersed at three different immersions. In this way a knowledge of the radial extent of the rotating stall cells was gained. For the second stall the hot wire anemometer probes were all set at the 10% immersion so that information was obtained from which the speed and number of rotating stall cells could be deduced.

RESULTS AND DISCUSSION

For the testing of this rotor two banks of air filters were in place in the inlet of the facility (fig. 4). No deterioration in performance due to dirt accumulation occurred during this testing.

Overall Performance

The compressor map obtained during testing of the rotor is shown in figure 9. The inlet total-temperature level was established as the arithmetic

average of 24 inlet temperatures measured in the low velocity region at the facility inlet screen (fig. 4). The rotor exit total-temperature and total-pressure ratio were established on the basis of fixed probe readings by a mass weighting routine, as follows. At each immersion, measurements from all circumferential locations were arithmetically averaged. The static pressure was assumed to vary linearly from hub to casing based on the measured average hub and casing values. With static pressure, total pressure, and total temperature known, static density and absolute velocity were computed at each immersion. The tangential velocity was obtained from the total-temperature rise and the Euler turbomachinery equation, and this together with the absolute velocity and the design meridional streamline angle, gave the axial velocity. The discharge total-temperature and total-pressure ratio were then obtained from the following equations:

$$T = \frac{\sum_{j=1}^5 T_j \rho_j V_z j A_j}{\sum_{j=1}^5 \rho_j V_z j A_j}, \quad (1)$$

$$\frac{P}{P_{in}} = \left\{ \frac{\sum_{j=1}^5 \left[\left(\frac{P_j}{P_{in}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right] \rho_j V_z j A_j}{\sum_{j=1}^5 \rho_j V_z j A_j} + 1 \right\}^{\frac{\gamma}{\gamma-1}}. \quad (2)$$

These quantities were used with the real gas properties of dry air to compute the rotor adiabatic efficiencies.

All points plotted on the map at 50% and 70% speeds were obtained, as described previously, from direct measurements of pressure difference across the rotor. For Rotor 1B (ref. 1), nozzle flows had been somewhat erratic at 50% design speed. The scatter in weight flow was eliminated for that rotor by establishing a correlation between nozzle flow and integrated flow and reading off the nozzle flow equivalent to the known integrated flow. Although the nozzle flows obtained in the testing of Rotor 2E at 50% design speed were not erratic, the procedure previously adopted was retained for consistency. At higher speeds the corrected weight flow was obtained directly from the calibrated venturi flow nozzles.

The maximum rotor adiabatic efficiency for Rotor 2E, of 0.931, was achieved at 70% corrected speed. At design speed the peak efficiency, of 0.884, occurred quite close to stall. A line of constant throttle position through

the Rotors 2 design point intersects the 100% speed line at a place where, for any reasonable application of this rotor, the rotor would operate much too close to the stall line. For conditions at design speed, judged to have adequate stall margin, a total-pressure ratio of 1.711 and an adiabatic efficiency of 0.869 were achieved at a flow of 225.9 lbs/sec. Rotor 2E was designed to deliver a total-pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec.

A complete listing of the overall performance data (green readings) appears in table 2. A number of readings were repeated in order to obtain a history of the performance over the period of testing time. On the basis of these measurements it was determined that repeatability was within acceptable limits. Only one typical reading, for each throttle valve setting, has been plotted.

Stall Performance

The throttle position representing the limit of stall-free performance of the rotor, upon closing the throttle valve, was recorded. With this information and performance data at throttle positions close to the stall throttle position it is possible to extrapolate each speed line on the compressor map to the limit of stall free operation. The stall line determined in this manner is shown in figure 9. The overall performance measurements, recorded while the rotor was operating with stall present, appear as solid symbols in figure 9. Since the flow was quite unsteady for these readings their accuracy is open to question.

Samples of the hot-wire anemometer data appear in figure 10. These are copies of Visicorder traces from the three anemometers. In figure 10(a) the anemometers are at immersions of 20%, 50% and 70%. A study of such traces gives an indication of the radial extent of stall cells. In figure 10(b) the anemometers are each at 10% immersion.

In order to establish the number and speed of the rotating stall cells, the phase difference between any two hot wires gives certain options and the use of a third anemometer eliminates all integral numbers except one. A knowledge of the paper speed of the trace and the number of cells permits deduction of the stall speed/rotor speed ratio. This method generally follows the method given in reference 6. Another method is available to check the number and speed of the rotating stall cells by utilizing the traces from a rotor strain gauge and a hot wire. The number of stall cells can be calculated by adding the number of pulses per unit time of the strain gauge and the hot wire and dividing the total by the number of rotor revolutions for the same unit of time. The ratio of stall speed to rotor speed is calculated by dividing the number of pulses per unit time on the hot-wire trace by the product of the rotor revolutions per unit time and the number of stall cells. The number and speed of the rotating stall cells determined by both methods were in agreement. These data and other stalling performance information are presented in figure 10(c).

Blade Element Performance

For presentation of the data from traverse probes located upstream and downstream of the rotor, a method of adjusting the data to obtain conditions at the blade edges was used. Knowing the measured total pressure, total temperature, static pressure and flow angle at each immersion and using the design meridional streamline angle, the meridional Mach number and all velocity components at each measurement plane may be calculated. Application of the condition of constant angular momentum along design streamlines yields the tangential velocity at each blade edge. It is assumed that the shape of each meridional stream tube, between a measurement plane and its adjacent blade edge, remains fixed at the design shape for all data conditions. The meridional Mach number at a measurement plane may then be used to determine the meridional Mach number at the blade edge by use of the relationship shown in figure 11. This method is not strictly correct at the trailing edge where there may be an appreciable swirl velocity together with a change in radius between the edge and the measurement plane. Nevertheless, since the radius changes are not large, the method should be a very good approximation. With the tangential velocities and the meridional Mach numbers at the edges thus obtained, and with measured stagnation conditions assumed to be constant along the design streamlines, the velocities, Mach numbers, and all of their components may be determined at the blade edges. The constant physical quantities used in these computations at the measurement planes and at the blade edges are given in table 3.

In order to check out this procedure and to determine small differences due to calculation technique, design values of total pressure, total temperature, static pressure and flow angle were used in a sample calculation. Treating this information as though it were test data, the calculation routine was used to give design point blade element performance, yielding the data listed in table 4. Table 5 is included to give a more complete description of the abbreviations used. Some indication of the small differences which can occur is given in table 4 by the comparison of the integrated flows, at the upstream and downstream measurement planes, with the nozzle flow. In this case the nozzle flow was set equal to the design flow.

Complete listings of blade element data are given in table 6 and graphs of some blade element data, plotted as a function of incidence angle, are presented in figure 12.

Measurements of discharge stagnation temperature taken from the fixed instrumentation were judged to be more reliable than those from the cobra traversing probes. Efficiency, loss coefficient and loss parameter were therefore processed by separate computation, using fixed instrumentation stagnation temperatures and pressures in conjunction with the inlet relative Mach number obtained from the traverse probe data. The results of this computation are given as an addition in table 6 and loss coefficients obtained in this way are shown in figure 12.

For most of the readings the part-span shroud wake impinged upon the center element. In the testing of Rotor 2E no substantial radial movement of the wake, upon closing the throttle valve, was observed. This is substantiated by figure 13 which illustrates the effect of throttle valve setting, upon two rotor exit angle traverses, at 90% speed.

REFERENCES

1. Seyler, D.R., and Gostelow, J.P.: Single Stage Experimental Evaluation of High Mach Number Compressor Rotor Blading, Part 2 - Performance of Rotor 1B, NASA CR-54582, September 22, 1967.
2. Seyler, D.R., and Smith, L.H., Jr.: Single Stage Experimental Evaluation of High Mach Number Compressor Rotor Blading, Part 1 - Design of Rotor Blading, NASA CR-54581, April 1, 1967.
3. Miller, Genevieve R., Lewis, George W., Jr., and Hartmann, Melvin J.: Shock Losses in Transonic Compressor Blade Rows, Journal of Engineering for Power, Trans. ASME, Series A, Vol. 83, July 1961, pp. 235.
4. Robbins, William H., Jackson, Robert J., and Lieblein, Seymour: Blade-Element Flow in Annular Cascades, Aerodynamic Design of Axial-Flow Compressors, NASA SP-36, Chapt, VII, 1965, pp. 227-254.
5. Smith, L.H., Jr., and Yeh, Hsuan: Sweep and Dihedral Effects in Axial-Flow Turbomachinery, Journal of Basic Engineering, Trans. ASME, Series D, Vol. 85, 1963, pp. 401-416.
6. Huppert, Merle C.: Preliminary Investigation of Flow Fluctuations During Surge and Blade Row Stall in Axial-Flow Compressors, NASA RM E52E28, 1952.

Table 1. - Cascade Projection Data for Rotor 2E Blade Setting.

ψ	$\frac{r_1}{r_t}$	β'_1	i	κ'_1	$\kappa'_{s1} - \kappa'_1$	$\frac{t_{e1}}{c_t}$
1.0	.9963	64.67	3.29	61.38	2.49	.0060
.9	.9600	62.87	3.68	59.19	2.96	.0063
.8	.9229	61.79	4.10	57.69	3.48	.0066
.7	.8840	60.74	4.52	56.22	4.10	.0069
.6	.8433	59.66	4.94	54.72	4.84	.0072
.5	.8005	58.55	5.35	53.20	5.45	.0076
.4	.7540	57.27	5.82	51.45	5.91	.0079
.3	.7046	56.20	6.10	50.10	6.36	.0083
.2	.6492	55.53	6.09	49.44	6.80	.0088
.1	.5850	56.18	5.90	50.28	7.23	.0093
0	.4995	61.18	5.70	55.48	7.56	.0100
ψ	$\frac{r_2}{r_t}$	β'_2	δ°	κ'_2	β'_{2e}	$\frac{t_{e2}}{c_t}$
1.0	.9801	54.58	4.96	49.62	53.33	.0060
.9	.9489	54.41	4.79	49.62	50.47	.0063
.8	.9159	53.00	4.61	48.39	48.09	.0066
.7	.8815	50.84	4.69	46.15	45.17	.0070
.6	.8454	47.78	4.76	43.02	41.66	.0074
.5	.8070	44.05	5.05	39.00	37.76	.0078
.4	.7675	39.12	5.73	33.39	32.78	.0082
.3	.7257	33.36	6.71	26.65	27.15	.0086
.2	.6824	26.32	8.21	18.11	19.68	.0091
.1	.6378	18.34	10.70	7.64	8.52	.0095
0	.5912	10.18	16.82	-6.64	-19.05	.0100
ψ	$\frac{t_m}{c_t}$	γ°	$\frac{a}{c_t}$	σ	ϕ_t	
1.0	.0350	57.40	.660	1.3058	11.76	
.9	.0387	55.58	.621	1.3520	9.57	
.8	.0426	53.85	.585	1.4036	9.30	
.7	.0467	51.83	.562	1.4618	10.07	
.6	.0510	49.30	.534	1.5283	11.70	
.5	.0556	46.10	.500	1.6055	14.20	
.4	.0604	42.42	.500	1.6963	18.06	
.3	.0655	38.37	.500	1.8044	23.45	
.2	.0708	33.77	.500	1.9382	31.33	
.1	.0770	28.96	.500	2.1106	42.64	
0	.0850	24.42	.500	2.3663	62.12	

Table 2. - Overall Performance based on Fixed Instrumentation

*Rdg.	Total press. ratio	Rotor adiab. eff.	Corrected weight flow lb/sec	Rotor speed, percent design	Throttle valve setting	Operating mode	**Pressure measurement system
1	1.153	.9462	121.90	49.96	10.0	Stall free	Abs.
2	1.331	.9467	167.71	70.04	10.0	Stall free	Abs.
3	1.652	.9056	203.58	89.96	10.0	Stall free	Abs.
4	1.857	.8848	220.08	99.96	10.0	Stall free	Abs.
5	1.173	.8948	101.28	49.96	4.2	Stall free	Abs.
6T	1.353	.8806	143.33	69.93	5.8	Stall free	Abs.
7T	1.672	.9026	198.52	90.03	9.0	Stall free	Abs.
8T	1.863	.8825	220.04	100.11	9.9	Stall free	Abs.
9T	1.979	.8316	233.40	110.13	10.9	Stall free	Abs.
11T	1.568	.8340	227.72	100.05	15.0	Stall free	Abs.
12T	1.617	.8481	226.51	100.08	14.0	Stall free	Abs.
13T	1.679	.8677	226.28	99.96	13.0	Stall free	Abs.
14T	1.728	.8747	225.74	100.04	12.3	Stall free	Abs.
15T	1.770	.8811	225.50	100.04	11.7	Stall free	Abs.
16T	1.815	.8870	223.67	100.06	11.0	Stall free	Abs.
17T	1.320	.8238	214.92	90.02	50.0	Stall free	Abs.
18T	1.501	.8927	215.33	90.09	14.0	Stall free	Abs.
19T	1.542	.9117	214.31	90.01	13.0	Stall free	Abs.
20T	1.592	.9194	213.11	90.05	12.0	Stall free	Abs.
21T	1.629	.9246	209.41	89.95	11.0	Stall free	Abs.
22T	1.663	.9167	204.67	90.06	10.0	Stall free	Abs.
23	1.606	.9132	211.72	90.02	11.7	Stall free	Abs.
24	1.777	.8785	225.38	100.11	11.7	Stall free	Abs.
25	1.814	.8775	223.09	100.07	11.0	Stall free	Abs.
26	1.689	.8651	226.78	100.08	13.0	Stall free	Abs.
27	1.921	.8253	234.43	110.00	11.7	Stall free	Abs.
28	1.371	.9538	184.14	75.03	11.7	Stall free	Abs.
29	1.314	.9555	171.94	70.04	11.7	Stall free	Abs.
30	1.219	.9448	146.00	60.03	11.7	Stall free	Abs.
31	1.148	.9444	122.28	50.07	11.7	Stall free	Abs.
32T	1.438	.7455	234.99	110.09	50.0	Stall free	Abs.
33T	1.373	.7856	225.73	99.99	50.0	Stall free	Abs.
34T	1.756	.8157	234.55	110.07	14.0	Stall free	Abs.
35T	1.824	.8220	234.86	109.94	13.0	Stall free	Abs.
36T	1.875	.8245	234.75	109.97	12.3	Stall free	Abs.
37T	1.921	.8285	233.35	109.95	11.7	Stall free	Abs.
38T	1.946	.8266	233.84	110.02	11.3	Stall free	Abs.
39T	1.218	.9254	185.64	70.02	50.0	Stall free	Abs.
40T	1.291	.9634	178.53	70.05	15.0	Stall free	Abs.
41T	1.311	.9646	172.54	70.02	12.3	Stall free	Abs.
42T	1.319	.9635	169.39	69.95	11.0	Stall free	Abs.
43T	1.341	.9461	161.84	69.94	9.0	Stall free	Abs.
44T	1.350	.9061	153.93	70.05	7.5	Stall free	Abs.
45T	1.116	.9624	142.8	49.98	50.0	Stall free	Abs.
46T	1.127	.9905	136.4	50.03	25.0	Stall free	Abs.

*The letter "T" following the reading number indicates Blade-Element Performance data were recorded.

**Abs. - Instrumentation arranged to record absolute pressure at rotor inlet and exit.

Diff. - Instrumentation arranged to record difference between rotor inlet and exit pressures.

Table 2. - Overall Performance based on Fixed Instrumentation. (cont'd)

*Rdg.	Total press. ratio	Rotor adiab. eff.	Corrected weight flow lb/sec	Rotor speed, percent design	Throttle valve setting	Operating mode	**Pressure measurement system
47T	1.137	.9810	131.69	50.04	18.0	Stall free	Abs.
48T	1.141	.9952	127.96	49.90	15.0	Stall free	Abs.
49T	1.151	.9630	122.9	50.06	11.0	Stall free	Abs.
50T	1.164	.9419	113.0	49.93	7.0	Stall free	Abs.
51T	1.172	.8883	102.5	50.02	4.2	Stall free	Abs.
52	1.137	.7414	90.19	50.04	3.3	Stalled	Abs.
53	1.300	.7552	129.36	70.08	4.9	Stalled	Abs.
54	1.575	.7927	182.12	90.15	8.0	Stalled	Abs.
55	1.745	.7960	202.53	100.02	9.3	Stalled	Abs.
56	1.898	.7727	217.72	110.27	10.1	Stalled	Abs.
57	1.117	.9628	142.8	50.03	50.0	Stall free	Abs.
58	1.128	.9245	136.4	50.05	25.0	Stall free	Abs.
59	1.137	.9646	131.69	50.05	18.0	Stall free	Abs.
60	1.142	.9460	127.96	50.04	15.0	Stall free	Abs.
61	1.151	.9485	122.9	50.01	11.0	Stall free	Abs.
62	1.164	.9115	113.0	50.02	7.0	Stall free	Abs.
63	1.172	.8827	102.5	49.98	4.2	Stall free	Abs.
64	1.217	.8996	185.18	70.02	50.0	Stall free	Abs.
65	1.291	.9482	178.42	70.02	15.0	Stall free	Abs.
66	1.311	.9447	172.51	69.98	12.3	Stall free	Abs.
67	1.322	.9487	169.85	70.04	11.0	Stall free	Abs.
68	1.346	.9370	161.01	70.03	9.0	Stall free	Abs.
69	1.351	.9047	152.06	69.98	7.5	Stall free	Abs.
70	1.353	.8697	142.96	70.02	5.8	Stall free	Abs.
71	1.811	.8729	223.83	100.12	11.0	Stall free	Abs.
72	1.777	.8782	225.61	100.11	11.7	Stall free	Abs.
73	1.729	.8659	226.03	99.96	12.3	Stall free	Abs.
74	1.687	.8625	226.47	100.24	13.0	Stall free	Abs.
75	1.127	.9525	136.4	50.01	25.0	Stall free	Abs.
76	1.113	.8752	142.8	50.02	50.0	Stall free	Diff.
77	1.123	.8800	136.4	50.07	25.0	Stall free	Diff.
78	1.132	.9078	131.69	50.04	18.0	Stall free	Diff.
79	1.138	.9393	127.96	50.01	15.0	Stall free	Diff.
80	1.147	.9235	122.9	50.02	11.0	Stall free	Diff.
81	1.159	.8855	113.0	50.03	7.0	Stall free	Diff.
82	1.167	.8526	102.5	50.00	4.2	Stall free	Diff.
83	1.213	.8801	186.45	70.03	50.0	Stall free	Diff.
84	1.284	.9262	177.45	69.99	15.0	Stall free	Diff.
85	1.303	.9016	171.43	70.11	12.3	Stall free	Diff.
86	1.316	.9344	169.29	70.03	11.0	Stall free	Diff.
87	1.338	.9159	160.27	70.10	9.0	Stall free	Diff.
88	1.345	.8821	151.44	70.03	7.5	Stall free	Diff.
89	1.347	.8569	143.58	70.08	5.8	Stall free	Diff.
90	1.122	.8945	136.4	50.03	25.0	Stall free	Diff.

*The letter "T" following the reading number indicates Blade-Element Performance data were recorded.

**Abs. - Instrumentation arranged to record absolute pressure at rotor inlet and exit.

Diff. - Instrumentation arranged to record differences between rotor inlet and exit pressures.

Table 3. - Constants Used in Data Analysis Methods
 Columns list data in order of increasing immersion number

Parameter	Plane 0.95	Edge 1	Edge 2	Plane 1.51	Plane 1.57
A_j	1.3108 1.1849 1.0814 1.0567 1.0967			1.0320 .9483 .8661 .7831 .7001	1.0067 .9206 .8285 .7593 .7043
r_j	18.323 17.473 15.733 14.023 12.191 10.023 8.550	18.182 17.392 15.759 14.180 12.456 10.494 9.116	17.887 17.201 15.768 14.354 12.921 11.516 10.789	17.838 17.148 15.770 14.391 13.012 11.634 10.944	17.836 17.166 15.817 14.501 13.198 11.864 11.169
ϵ_j°	-1.57 1.85 6.10 11.76 20.40	-4.50 1.00 5.70 12.25 22.20	-4.00 -0.50 3.00 7.00 13.40	-6.68 .28 2.51 5.68 9.72	.07 .32 .42 .33 .13
$\kappa_j^\circ (\kappa_j^\circ s_j)$		58.90 (61.96) 55.46 (59.90) 52.25 (57.96) 49.71 (56.28) 50.60 (57.88)	49.44 44.73 36.17 23.45 5.78		σ_j (Used for Diffusion Factor)

+ first and last values are casing and hub radii, respectively.

Radii are in inches.
 Areas are in square feet.

Frontal Area = 7.2660
 Annulus Area = 5.4495

$\left(\frac{w}{w^*}\right)_1$	$\left(\frac{w}{w^*}\right)_2$
$\left(\frac{w}{w^*}\right)_U$	$\left(\frac{w}{w^*}\right)_d$

Table 4. - Listing of Check Case for Blade Element Results Using Design Data.

RADIAL POSITION	REL. INLET FLOW ANG.	INCL ANG MN.CMBR,LN	INCL ANG SUCT SURF	INLET REL MACH NO.	INLET REL MACH NO.	INLET ABS VELOCITY	INLET ABS MACH NO.
1	6.2,.022	3./25	0.665	1.4012	1203.455	1334.214	694.000
2	6.0,159	4.599	0.259	1.2991	1393.785	1208.940	693.614
3	5./9.7	2./0/	-0.003	1.1964	1282.123	108/.808	684.262
4	5.6,725	6.015	-0.555	1.0823	1164.969	925.255	666.587
5	5.5,874	6.274	-1.006	1.9055	984.885	805.039	651.214
6						567.370	525.312
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT INLET	ROTOR SPD AT EXIT	ROTOR SPD AT EXIT	ROTOR SPD AT EXIT
1	54.224	4.784	8.401	1.8352	982.726	1319.562	777.260
2	44.576	4.545	10.784	0.7355	864.366	1209.630	889.432
3	4.761	2.291	16.196	0.646/	757.639	1101.156	822.263
4	30.261	7.111	25.165	0.5945	692.226	991.222	826.914
5	1.164	11.384	39.710	6.6221	.09/.45	883.441	960.917
RADIAL POSITION	DIFFUSION ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET ABS TANG. VEL
1	0.4/1	0.53999	0.4556	0.	220.202	1334.214	799.060
2	0.213	0.41649	0.498/	0.	223.591	1208.941	656.040
3	0.222	0.4/039	0.5299	0.	296.801	108/.808	204.356
4	0.254	0.51484	0.52/6	0.	639.696	925.223	551.229
5	0.448	0.47317	0.383/	0.	679.209	805.039	204.333
RADIAL POSITION	ADIABATIC POLYTROPIC EFFICIENCY	TOT. PRESS RATIO	TOT. TEMP RATIO	ABS-INLET FLOW ANG.	Abs-Exit FLOW ANG.	Abs-Exit FLOW ANG.	Abs-Exit FLOW ANG.
1	3./951	0.8116	1.760	1.220	U.	42.113	0.833
2	0.817/	0.8316	1.760	1.215	U.	44.229	0.811
3	0.8321	0.8449	1.760	1.211	0.	46.275	0.830
4	0.8628	0.8755	1.760	1.205	0.	47.027	0.914
5	0.9106	0.9174	1.760	1.193	U.	45.769	1.259
TRAVERSE POSITION	TRAVERSE PRESSURE RATIO	1.7609	FIXED INSTRUMENTATION	PRESSURE RATIO =	1. /6.0		
1	TRAVERSE ADIABATIC EFF.	0.8376		ADIABATIC EFF. =	0.830		
2	TRAVERSE POLYTROPIC EFF.	0.8500		POLYTROPIC EFF. =	0.850		
3	FLOW COEFFICIENT L.E.	0.980		NOZZLE WEIGHT FLOW =	217.49		
4	FLOW COEFFICIENT T.E.	0.950	L.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW =	0.0324			
5			T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW =	1.00408			

Table 5. - Simulated Listing for Symbolic Identification of Column Headings.

RADIAL POSITION 1	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUET.SURF	INLET REL MACH NO.	INLET REL VELOCITY	MOTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
2	β_1^i	i	$\beta_1^i - \kappa_{s1}^i$	M_1^i	V_1^i	V_1	V_1	M_1	V_{z1}
3									
4									
5									
RADIAL POSITION 1	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELOCITY	MOTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
2	β_2^i	δ^o	$\Delta\beta^i$	M_2^i	V_2^i	V_2	V_2	M_2	V_{z2}
3									
4									
5									
RADIAL POSITION 1	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG.VEL	EXIT ABS TANG.VEL	INLET REL TANG.VEL	EXIT REL TANG.VEL	AXIAL VEL. RATIO	
2	D	C_p	C_h	$V_{\theta 1}$	$V_{\theta 2}$	$V'_{\theta 1}$	$V'_{\theta 2}$		$\frac{V_{z2}}{V_{z1}}$
3									
4									
5									
RADIAL POSITION 1	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS RATIO	TOT. TEMP RATIO		ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.		
2									
3									
4									
5									
TRAVERSE PRESSURE RATIO						FIXED INSTRUMENTATION	PRESSURE RATIO		
TRAVERSE ADIABATIC EFF.							ADIABATIC EFF.		
TRAVERSE POLYTROPIC EFF.							POLYTROPIC EFF.		
FLOW COEFFICIENT L.E.							NOZZLE WEIGHT FLOW		
FLOW COEFFICIENT T.E.							L.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	
							T.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION 1	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO		TOT. TEMP RATIO			
2	$\frac{\bar{\omega}' \cos \beta_2^i}{2\sigma}$	η_{ad}	$\bar{\omega}'$	$\frac{P_{1.57}}{P_{0.05}}$		$\frac{T_{1.57}}{T_{0.05}}$			
3									
4									
5									

Table 6. - Listine of Blade Element Performance

NASA = TASK 1 (ROTAR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 6 READING NUMBER 6 DATE 4/13/1967

RADIAL POSITION	RFL. INLFIT FLOW ANG.	INCID ANG MN CMBR LIN	INLET REL MACH NO.	INLET REL VELOCITY	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET AX. VELOCITY
1	67.359	8.459	5.399	0.9159	1011.350	932.980	0.353
2	64.821	9.361	4.921	0.8467	934.163	845.379	0.360
3	62.834	10.586	4.976	0.7764	855.062	760.674	0.356
4	60.377	10.667	4.097	0.7012	773.074	668.192	0.353
5	60.869	10.269	2.989	0.5941	697.052	562.942	0.306
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT VELocITY	EXIT ABS VELOCITY	EXIT AX. VELOCITY
1	53.766	4.326	13.593	0.5599	644.688	922.734	0.479
2	49.646	4.916	15.175	0.5270	605.255	845.861	0.478
3	44.847	8.677	17.989	0.4296	492.582	700.009	0.478
4	31.882	8.432	28.495	0.4406	501.494	693.136	0.532
5	16.819	11.039	44.051	0.4289	485.072	617.766	0.592
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANg. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	AXIAL VEL RATIO
1	0.508	0.36155	0.4262	0.	403.169	519.565	0.976
2	0.490	0.43327	0.4738	0.	384.626	845.379	0.986
3	0.575	0.48689	0.5028	0.	422.872	760.674	347.137
4	0.504	0.56331	0.5349	0.	429.690	668.192	263.446
5	0.441	0.58900	0.4594	0.	480.927	562.942	1.115
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	REL. TEMP	ABS. EXIT FLOW ANG.	ABS. INLET FLOW ANG.
1	0.7425	0.7532	1.352	1.121	46.639	0.	46.639
2	0.8441	0.8506	1.346	1.105	44.463	0.	44.463
3	0.8099	0.8174	1.327	1.104	50.467	0.	50.467
4	0.9179	0.9214	1.357	1.099	45.413	0.	45.413
5	0.9652	0.9667	1.376	1.099	46.732	0.	46.732
TRAVERSE POSITION	TRAVERSE PRESSURE RATIO	= 1.3516	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.3530		
1	TRAVERSE ADIABATIC EFF.	= 0.8463		ADIABATIC EFF.	= 0.8806		
2	TRAVERSE POLYTROPIC EFF.	= 0.8527		POLYTROPIC EFF.	= 0.8856		
3	FLOW COEFFICIENT L.E.	= 0.980		NOZZLE WEIGHT FLOW	= 143.33		
4	FLOW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 0.98309		
5	PERCENT DESIGN SPEED	= 70	T.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 0.95937		
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION							
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO		
1	0.0666	0.7482	0.2147	1.347	1.119		
2	0.0249	0.8667	0.1150	1.350	1.103		
3	0.0253	0.8765	0.1176	1.338	1.099		
4	0.0100	0.9604	0.0435	1.357	1.095		
5	0.0027	0.9919	0.0120	1.374	1.096		

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTOR 2F)

N.A.S.A. COMPRESSOR OUTPUT DATA

POINT NUMBER
7 READING NUMBER
3-LADE ELEMENT PERFORMANCE RESULTS
DATE 4/13/1967

RADIAL POSITION	TOT. INLET FFL. INLET FFL. INCID ANG. MN.CMBR.LN.	INCID ANG. SLCT SURF	INLET REL. MACH NO.	INLET SPD AT INLET VELOCITY	INLET ABS MACH NO., VELOCITY
1 6.414	4.514	1.454	1.2346	12n1.133	0.554 601.181
2 6n.272	4.812	0.372	1.1579	1253.481	0.574 621.549
3 5n.208	5.958	0.248	1.0661	1153.888	0.564 607.073
4 5n.324	6.614	0.044	0.9600	1041.293	0.541 573.255
5 57.292	6.692	-0.588	0.8068	8n2.101	0.460 465.464

RADIAL POSITION	REL. EXIT FFL. EXIT ANG. T.E.	RFL. TURV ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT VELOCITY	EXIT ABS MACH NO., VELOCITY
1 52.134	2.698	1.1.276	0.7028	834.706	0.621 511.834
2 47.866	3.136	12.406	0.6612	775.097	0.624 519.977
3 42.041	5.871	16.167	0.5875	6n5.315	0.632 508.574
4 32.395	8.945	23.929	0.5595	645.352	0.671 542.014
5 12.909	13.129	38.384	0.5201	595.658	0.724 549.725

RADIAL POSITION	S1. PRESS FACTOR	S1. PRESS RISE COEFF	CH1 TANg. VEL	INLET ARS TANG. VEL	INLET REL TANG. VEL
1 0.523	0.41485	0.5140	0.	529.681	1201.265 0.851
2 0.519	0.49379	0.5654	0.	514.310	1088.474 0.837
3 0.547	0.55933	0.6020	0.	532.847	979.412 0.838
4 0.525	0.61770	0.6132	0.	548.547	860.336 0.946
5 0.493	0.63362	0.5298	0.	607.104	724.820 1.181

RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	ARS. INLET FLOW ANG.
1 0.8061	0.8204	1.725	1.209	0.	45.982
2 0.8820	0.4906	1.705	1.187	0.	44.686
3 0.8783	0.8868	1.673	1.181	0.	46.335
4 0.9358	0.9402	1.661	1.167	0.	45.343
5 0.9304	0.9351	1.642	1.164	0.	47.840

TRAVERSE PRESSURE RATIO = 1.6849
 TRAVERSE ADIABATIC EFF. = 0.8770
 TRAVERSE POLYTROPIC EFF. = 0.8957
 F-LW COEFFICIENT L.E. = 0.980
 F-LW COEFFICIENT T.E. = 0.950
 PERCENT DESIGN SPEED = 90
 L.E. CHECK WEIGHT FLOW/NOCZ. WEIGHT FLOW = 0.999928
 T.E. CHECK WEIGHT FLOW/NOCZ. WEIGHT FLOW = 0.988865

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0424	0.7964	0.1383	1.695	1.204
2	0.0153	0.9017	0.0681	1.704	1.182
3	0.0193	0.9143	0.0857	1.669	1.172
4	0.0043	0.9828	0.0187	1.654	1.157
5	0.0090	0.9711	0.0405	1.625	1.153

Table 6. - Listing of Blade Element Performance (continued).

NASA » TASK 1 (ROTAR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS
POINT NUMBER 8 READING NUMBER 8 DATE 4/13/1967

RADIAL POSITION	RFL. INLET FLOW ANG. MN.CMBR.LN	INCID ANG SLCT SURF	INLET REL. MACH NO.	INLET RFL. VEL. 1504.684	MOTOR SPD AT INLET VEL. 1335.697	INLET ABS MACH NO. VELOCITY	INLET ABS MACH NO. VELOCITY
1	62.657	3.757	0.697	1.3977	1210.284	692.811	690.675
2	59.630	4.170	0.270	1.3095	1402.826	709.320	664.662
3	57.335	5.085	-0.525	1.2090	1295.492	701.670	655.655
4	55.263	5.553	*1.017	1.0932	1172.961	678.769	633.633
5	56.317	5.717	*1.563	0.9160	993.033	805.934	801.159
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN	EXIT REL. MACH NO.	ROTOR SPD	EXIT ABS VFLOCITY	EXIT ABS MACH NO. VELOCITY
1	51.594	2.154	11.063	0.7388	891.760	1321.028	834.139
2	47.446	2.716	12.184	0.7108	842.843	1210.975	820.459
3	42.911	6.741	14.423	0.5951	704.546	1102.380	809.183
4	31.295	7.845	23.967	0.5972	695.769	992.327	869.159
5	20.064	14.284	*6.253	0.5494	634.179	884.423	899.354
RADIAL POSITION	DIFFUSION ST. PRESS FACTOR	CH1 RISE COEFF	INLET ARS TANG. VEL	EXIT ARS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.558	0.39624	0.5139	0.	622.874	1335.697	698.155
2	0.540	0.48628	0.5746	0.	590.115	1210.284	620.860
3	0.603	0.56151	0.6184	0.	623.051	1089.017	479.349
4	0.555	0.62528	0.6331	0.	632.884	956.615	359.443
5	0.527	0.63938	0.5472	0.	672.110	805.934	212.313
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	INLET REL FLOW ANG.	ABS. EXIT FLOW ANG.	
1	0.7577	0.7790	1.937	1.275	0.	48.377	
2	0.8753	0.8863	1.928	1.236	0.	45.994	
3	0.8424	0.8555	1.862	1.231	0.	50.368	
4	0.9203	0.9270	1.877	1.215	0.	46.946	
5	0.8935	0.9020	1.795	1.204	0.	49.143	
TRAVERSE POSITION	TRAVERSE ADIABATIC EFF.	= 1.8865	FIXED INSTRUMENTATION	PRESSURE RATIO	AIRS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	
1	TRAVERSE POLYTROPIC EFF.	= 0.8470		ADIABATIC EFF.	= 0.	1.8630	
2	FLOW COEFFICIENT L.E.	= 0.8500		POLYTROPIC EFF.	= 0.	0.8825	
3	FLOW COEFFICIENT T.E.	= 0.980		NOZZLE WEIGHT FLOW	= 0.	0.8923	
4	PERCENT DESIGN SPEED	= 100	L.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 220.04		
5			T.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 0.99069		
					0.98582		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0491	0.7783	0.2155	1.896	1.258
2	0.0235	0.8947	0.1039	1.915	1.228
3	0.0285	0.8774	0.1282	1.849	1.219
4	0.0090	0.9660	0.0388	1.859	1.201
5	0.0161	0.9472	0.0734	1.768	1.187

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTAR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS
POINT NUMBER 9 READING NUMBER 9 DATE 4/13/1967

RADIAL POSITION	RFL. INLFT FLOW ANG.	INCID ANG MN.CMBR.LN	INLET REL SLCT.SURF	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.
1	62.422	3.522	0.462	1.5572	1469.363	769.813	0.723
2	59.744	4.284	-0.156	1.4524	1541.417	1331.399	0.732
3	57.605	5.355	-0.355	1.3373	1420.825	1197.997	0.719
4	55.408	5.598	-0.472	1.2100	1288.015	1052.345	0.698
5	54.410	5.910	-1.470	1.0121	1091.096	886.586	0.590
RADIAL POSITION	RFL. EXIT FLOW ANG.	RFL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT			
1	50.116	0.676	12.306	0.8316	1012.321	1453.226	938.727
2	46.173	1.443	13.571	0.8059	940.843	1332.159	922.518
3	45.108	8.938	12.497	0.6178	740.347	1212.698	864.597
4	26.045	2.595	29.363	0.6526	764.226	1091.631	1023.536
5	19.421	13.641	16.389	0.6505	751.562	972.929	1018.329
RADIAL POSITION	ST. PRESS	CHI.	INLET ABS TANG. VEL.	INLET ABS TANG. VEL.	INLET REL TANG. VEL.	INLET REL TANG. VEL.	INLET REL TANG. VEL.
1	RISE COEFF 0.539	0.31764	0.4504	0.	677.211	1469.363	766.016
2	0.515	0.40447	0.5107	0.	638.989	1331.399	693.171
3	0.627	0.47666	0.5517	0.	688.587	1197.997	524.111
4	0.568	0.51592	0.5423	0.	758.011	1052.345	333.620
5	0.475	0.54668	0.4676	0.	729.108	886.586	243.821
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP RATIO	ARS. INLET FLOW ANG.	ARS. EXIT FLOW ANG.	AXIAL VEL.RATIO
1	0.6942	0.7229	2.040	1.325	0.	0.	0.845
2	0.8261	0.8428	2.062	1.278	0.	0.	0.857
3	0.7446	0.7667	1.917	1.275	0.	0.	0.87
4	0.8523	0.9666	2.080	1.273	0.	0.	0.91
5	0.832	0.8938	1.969	1.242	0.	0.	1.174
TRAVERSE PRESSURE RATIO	= 2.0199	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.9790			
TRAVERSE ADIABATIC EFF.	= 0.7895		ADIABATIC EFF.	= 0.8316			
TRAVERSE POLYTROPIC EFF.	= 0.8092		POLYTROPIC EFF.	= 0.8469			
FLW COEFFICIENT L.E.	= 0.980		NOZZLE WEIGHT FLOW	= 233.40			
FLW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 0.98462				
PERCENT DESIGN SPEED	= 110	T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 1.03121				

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0590	0.7405	0.2509	1.995	1.295
2	0.0336	0.8540	0.1451	2.037	1.264
3	0.0446	0.7996	0.2087	1.909	1.254
4	0.0397	0.8003	0.1634	1.955	1.245
5	0.0179	0.9440	0.0813	1.982	1.229

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA									
POINT NUMBER		BLADE ELEMENT PERFORMANCE RESULTS		NUMBER 11		DATE		4/13/1967	
RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMRR.LN	INLET REL SLCT.SURF	INLET RFL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY	
1	61.137	2.237	*0.823	1.4269	1336.195	738.762	0.690	736.485	
2	59.514	3.054	-1.386	1.3309	1419.836	741.657	0.695	741.544	
3	54.808	4.558	*1.152	1.2191	1303.775	1089.423	716.232	712.691	
4	54.590	4.880	*1.590	1.1045	1143.422	956.971	696.199	680.347	
5	55.600	5.000	*2.280	0.9242	1002.755	806.234	596.242	552.043	
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT VFLDCTY	EXIT ABS VFLDCTY	EXIT ABS MACH NO.	EXIT AX. VELOCITY	
1	54.728	5.288	6.409	1.0165	1321.520	770.608	0.666	678.511	
2	50.749	6.019	7.764	0.9222	1042.747	1211.426	0.674	672.406	
3	49.488	12.318	8.319	0.7133	830.070	1102.791	731.475	549.815	
4	30.281	6.831	24.308	0.7908	896.230	992.696	946.802	835	
5	17.168	11.388	18.432	0.7815	875.012	884.753	1050.148	0.938	
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO	
1	0.316	0.24114	0.3473	0.	362.228	1336.195	959.293	0.921	
2	0.343	0.30773	0.3942	0.	388.464	1210.734	822.962	0.907	
3	0.476	0.33668	0.3962	0.	481.591	1089.423	621.200	0.771	
4	0.369	0.33574	0.3501	0.	543.294	956.971	449.402	1.131	
5	0.282	0.19545	0.0973	0.	632.918	806.234	251.835	1.477	
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	ARS. INLET FLOW ANG.	ARS. EXIT FLOW ANG.			
1	0.7872	0.7995	1.524	1.163	0.	28.096			
2	0.8303	0.8405	1.553	1.162	0.	30.016			
3	0.6476	0.6656	1.450	1.173	0.	41.216			
4	0.8688	0.8777	1.648	1.177	0.	35.219			
5	0.8388	0.8497	1.643	1.182	0.	37.826			
TRAVERSE POSITION	PRESSURE RATIO	1.5628	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.5680				
1	TRAVERSE ADIABATIC EFF.	# 0.8002	LOSS COEFFICIENT	ADIABATIC EFF.	= 0.8340				
2	TRAVERSE POLYTROPIC EFF.	# 0.8124		POLYTROPIC EFF.	= 0.8442				
3	FLCW COEFFICIENT L.E.	# 0.980		NOZZLE WEIGHT FLOW	= 227.72				
4	FLCW COEFFICIENT T.E.	# 0.950	L.F. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW	# 0.97827				
5	PERCENT DESIGN SPEED = 100		T.E. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW	# 0.99942				

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0320	0.7749	0.1510	1.523	1.165
2	0.0288	0.3152	0.1359	1.557	1.165
3	0.0385	0.1543	0.1915	1.486	1.159
4	0.0153	0.9312	0.0655	1.652	1.166
5	0.0296	0.8945	0.1323	1.639	1.170

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 12 READING NUMBER 12 DATE 4/13/1967

RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	SLCT.SURF	INLET REL		INLET SPD	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
				MACH NO.	VEL				
1	61.260	2.360	0.700	1.4243	1335.349	1524.052	734.558	0.686	732.294
2	58.629	3.169	-1.271	1.3284	1417.184	1209.968	737.827	0.692	737.714
3	54.512	4.262	-1.448	1.2241	1307.412	1088.733	723.868	0.678	720.289
4	54.328	4.618	-1.952	1.1092	1186.648	956.366	702.494	0.657	686.499
5	55.582	4.982	-2.298	0.9251	1002.355	805.724	596.259	0.550	552.058
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VEL	ROTOR SPD AT EXIT VFLOCITY	ROTOR SPD AT EXIT VFLOCITY	ROTOR SPD AT EXIT VFLOCITY	ROTOR SPD AT EXIT VFLOCITY
1	54.346	4.906	6.914	0.9740	1134.972	1320.684	773.608	0.664	661.021
2	50.209	5.479	8.421	0.8929	1033.777	1210.659	781.721	0.675	661.601
3	47.115	10.945	9.397	0.6938	810.500	1102.093	750.565	0.643	551.217
4	39.157	8.707	22.172	0.7426	849.279	992.068	901.898	0.789	715.144
5	17.334	11.551	38.251	0.7490	841.849	884.193	1028.627	0.915	783.621
RADIAL POSITION	ST. PRESS RISE COEFF	CH1	INLET ARS TANG. VEL	INLET ARS TANG. VEL	INLET ARS TANG. VEL	INLET REL TANG. VEL	INLET REL TANG. VEL	INLET REL TANG. VEL	INLET REL TANG. VEL
1	0.351	0.26976	0.3803	0.	399.230	1335.349	921.454	0.903	0.893
2	0.369	0.34031	0.4292	0.	416.339	1209.968	794.320	0.897	0.897
3	0.499	0.37530	0.4376	0.	508.599	1088.733	593.494	0.765	0.765
4	0.410	0.42097	0.4394	0.	542.475	956.366	449.593	1.042	1.042
5	0.316	0.26045	0.1691	0.	639.657	805.724	244.536	1.419	1.419
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS RATIO	TOT. TEMP RATIO	TOT. TEMP RATIO	ABS. INLET FLOW ANG.	Abs. Inlet flow ang.	Abs. Inlet flow ang.	Abs. Inlet flow ang.
1	0.7836	0.7972	1.587	1.180	1.180	0.	31.130	31.130	31.130
2	0.8478	0.8578	1.617	1.174	1.174	0.	32.182	32.182	32.182
3	0.6785	0.9968	1.518	1.187	1.187	0.	42.697	42.697	42.697
4	0.8701	0.8792	1.679	1.184	1.184	0.	37.182	37.182	37.182
5	0.8493	0.8598	1.669	1.186	1.186	0.	39.224	39.224	39.224
TRAVERSE PRESSURE RATIO	= 1.6159	FIXED INSTRUMENTATION	PRESSURE RATIO	ADIABATIC EFF.	ADIABATIC EFF.	= 1.6170	= 0.8481	= 0.8481	= 0.8481
TRAVERSE ADIABATIC EFF.	= 0.8084	TRAVERSE POLYTROPIC EFF.	= 0.8209	TRAVERSE POLYTROPIC EFF.	TRAVERSE POLYTROPIC EFF.	= 0.8581	= 0.8581	= 0.8581	= 0.8581
TRAVERSE COEFFICIENT L.E.	= 0.980	FLOW COEFFICIENT L.E.	= r.950	NOZZLE WEIGHT FLOW	NOZZLE WEIGHT FLOW	= 226.51	= 0.98567	= 0.98567	= 0.98567
FLOW COEFFICIENT T.E.	= 100	PERCENT DESIGN SPEED	= 100	L.E. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW/NCZ.	T.E. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW/NCZ.	WEIGHT FLOW/NCZ.	WEIGHT FLOW/NCZ.
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1	0.0352	0.7721	0.1647	1.578	1.180				
2	0.0264	0.8413	0.1231	1.617	1.175				
3	0.0368	0.7834	0.1786	1.548	1.170				
4	0.0130	0.9416	0.0569	1.687	1.171				
5	0.0241	0.9151	0.1080	1.668	1.172				

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTAR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 13 READING NUMBER 13 DATE 4/13/1967

RADIAL POSITION	INLET ANG MN-CMBR.LN	INCID ANG SLCT.SURF	INLET REL MACH NO.	INLET REL VEL/LOCITY	ROTOR SPD AT INLET	INLET ABS VFLOCITY	INLET ABS VFLOCITY	INLET AX. VELOCITY
1 61.196	2.296	-0.764	1.4239	1523.175	1333.759	735.629	0.688	733.362
2 58.549	3.089	-1.351	1.3277	1416.710	1208.527	739.275	0.693	739.163
3 56.735	4.483	-1.225	1.2162	1362.494	1087.437	716.919	0.671	713.374
4 54.797	5.087	-1.483	1.0097	1178.149	955.227	689.621	0.644	673.910
5 55.615	5.015	-2.265	0.9230	1000.722	804.765	594.809	0.549	550.716
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	EXIT REL. ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ABS VFLOCITY	EXIT ABS VFLOCITY	EXIT AX. VELOCITY
1 53.733	4.293	7.463	0.9340	1097.548	1319.112	782.333	0.666	648.697
2 49.484	4.754	9.065	0.8511	990.713	1209.218	788.846	0.678	643.621
3 45.251	0.081	11.484	0.6646	779.672	1100.781	775.493	0.661	548.520
4 30.775	7.325	24.022	0.7113	816.563	990.887	908.404	0.791	697.706
5 17.754	11.974	37.961	0.6944	787.131	883.140	993.008	0.876	731.061
RADIAL POSITION	DIFFUSION ST. PRESS RISE COEFF	CH1	INLET ARS TAN ³ . VEL	EXIT ARS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	INLET REL TANG. VEL	AXIAL VEL. RATIO
1 0.384	C.30259	0.4172	0.	434.947	1333.759	1384.164	0.885	0.885
2 0.408	C.38033	0.4712	0.	456.069	1208.527	753.149	0.871	0.871
3 0.529	C.42138	0.4841	0.	547.438	1087.437	553.542	0.769	0.769
4 0.441	C.45801	0.4749	0.	575.383	955.227	415.504	1.035	1.035
5 0.372	C.355944	0.2741	0.	649.063	804.765	234.077	1.327	1.327
RADIAL POSITION	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP RATIO	TOT. TEMP RATIO	ARS. INLET FLOW ANG.	ARS. INLET FLOW ANG.	ARS. INLET FLOW ANG.	AUX. EXIT FLOW ANG.
1 0.7766	0.7920	1.662	1.201	0.	33.842	0.	33.842	0.
2 0.2697	0.8790	1.692	1.187	0.	35.321	0.	35.321	0.
3 0.7235	0.7414	1.612	1.202	0.	44.943	0.	44.943	0.
4 0.8833	0.8920	1.738	1.194	0.	39.512	0.	39.512	0.
5 0.8569	0.8691	1.698	1.190	0.	41.600	0.	41.600	0.
TRAVESE PRESSURE RATIO	= 1.6806	FIXED INSTRUMENTATION	PRESSURE RATIO	PRESSURE RATIO	= 1.6790			
TRAVESE ADIABATIC EFF.	= C.8216					ADIABATIC EFF. = 0.8677		
TRAVESE POLYTROPIC EFF.	= C.8342					POLYTROPIC EFF. = 0.8770		
FLW COEFFICIENT L.E.	= C.930					NOZZLE WEIGHT FLOW = 226.28		
FLW COEFFICIENT T.E.	= C.950					WEIGHT FLOW = 0.9829		
PERCENT DESIGN SPEED	= 100	L.E. CHECK WFIGHT FLOW/NCZ.				WEIGHT FLOW = 1.31149		
		T.E. CHECK WFIGHT FLOW/NCZ.				WEIGHT FLOW = 1.31149		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1 0.0366	0.7810	0.1687	1.642	1.195	1.195
2 0.0224	0.8743	0.1030	1.691	1.185	1.185
3 0.0328	0.8275	0.1537	1.641	1.184	1.184
4 0.0113	0.9227	0.0485	1.736	1.179	1.179
5 0.0223	0.9232	0.1000	1.693	1.176	1.176

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK I (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 14 READING NUMBER 14 DATE 4/13/1967

RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INLET REL SLCT.SURF	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.
1	61.451	2.551	*0.509	1.4188	1520.661	1334.823	0.680
2	58.623	3.163	-1.277	1.3266	1416.718	1209.492	0.691
3	56.575	4.325	-1.385	1.2226	1305.944	1088.304	0.676
4	54.385	4.675	-1.895	1.1075	1185.321	955.989	0.655
5	55.172	4.572	-2.708	0.9310	1007.461	805.407	0.559
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T,E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.
1	52.817	3.377	8.534	0.8974	1061.239	1320.164	0.676
2	48.791	4.061	9.932	0.8221	961.098	1210.182	0.683
3	44.461	8.291	12.114	0.6449	759.222	1101.659	0.668
4	31.212	7.762	23.172	0.6848	790.567	991.677	0.775
5	20.516	14.736	34.656	0.6372	78.940	803.844	0.816
RADIAL POSITION	ST. PRESS DIFFUSION FACTOR	CH1 RISE COEFF	CH1 TAN ³ .VEL	INLET ARS TAN ³ .VEL	EXIT ARS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL
1	0.416	0.32483	0.4410	0.	475.414	1334.823	0.882
2	0.437	0.40849	0.4999	0.	487.146	1209.492	0.858
3	0.552	0.45737	0.5304	0.	570.257	1088.304	0.754
4	0.468	0.52573	0.5424	0.	584.239	955.989	0.982
5	0.430	0.49212	0.4110	0.	634.510	805.407	1.189
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP RATIO	ARS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	AXIAL VEL. RATIO
1	0.7811	0.7973	1.731	1.218	0.	36.572	
2	0.9715	0.9813	1.753	1.200	0.	37.574	
3	0.7571	0.7744	1.689	1.214	0.	46.482	
4	0.9023	0.9100	1.793	1.201	0.	40.985	
5	0.8641	0.8740	1.715	1.193	0.	43.599	
TRAVERSE POSITION	TRAVERSE PRESSURE RATIO	TRAVERSE ADIABATIC EFF.	TRAVERSE POLYTROPIC EFF.	TRAVERSE WEIGHT FLOW	FIXED INSTRUMENTATION	PRESSURE RATIO	ADIABATIC EFF.
1	= 1.7378	= r.8319	= r.8445	= r.980	= r.95n	= 1.7280	= 0.8747
2							
3							
4							
5							
PERCENT DESIGN SPEED	= 100	L.E. CHECK WEIGHT FLOW/NCZ.	T.E. CHECK WEIGHT FLOW	= 1.00330	WEIGHT FLOW/NCZ. WEIGHT FLOW	= 0.98799	
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION							
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO		
1	0.0394	0.7831	0.1776	1.701	1.209		
2	0.0216	0.8860	0.0978	1.749	1.195		
3	0.0301	0.8507	0.1393	1.707	1.194		
4	0.0097	0.9602	0.0418	1.775	1.186		
5	0.0232	0.9188	0.1060	1.703	1.179		

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR INPUT DATA									
		BLADE ELEMENT PERFORMANCE RESULTS							
		POINT NUMBER		READING NUMBER	15	DATE	15	4/13/1967	
RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	SLECT SURF	INLET REL MACH NO.	INLET RFL VELCITY	ROTOR SPD AT INLET	INLET ABS VFLNCITY	INLET AX. MACH NO.	INLET AX. VELOCITY
1	61.448	2.548	*0.512	1.4178	1.520.678	1.334.793	728.554	0.679	726.308
2	58.682	3.222	*1.218	1.3243	1.415.806	1.209.464	736.005	0.688	735.893
3	56.895	4.645	*1.065	1.2149	1.301.109	1.088.280	713.114	0.666	709.588
4	54.820	5.110	*1.460	1.0985	1.178.711	955.967	689.555	0.643	673.855
5	55.751	5.151	*2.129	0.9214	999.713	805.389	592.263	0.546	548.359
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	RFL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT VELCITY	ROTOR SPD AT EXIT VELCITY	ROTOR SPD AT EXIT VELCITY	ROTOR SPD AT EXIT VELCITY	ROTOR SPD AT EXIT VELCITY
1	52.230	2.790	9.217	0.8574	1021.274	1320.134	810.078	0.680	624.945
2	48.126	3.396	10.556	0.7958	915.438	1210.155	808.525	0.688	624.393
3	43.537	7.367	13.358	0.6379	752.556	1101.634	799.149	0.677	545.158
4	30.427	6.977	24.393	0.66669	771.974	991.655	899.019	0.777	661.953
5	2n.021	14.241	35.780	0.60668	696.545	803.824	924.644	0.805	638.648
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VFL	EXIT ABS TANG. VFL	INLET REL TANG. VFL	EXIT REL TANG. VFL	INLET REL TANG. VFL	AXIAL VEL. RATIO
1	0.452	0.34807	0.4658	0.	513.576	1334.793	806.558	0.	0.860
2	0.461	0.43413	0.5254	0.	513.630	1209.464	696.525	0.	0.848
3	0.558	0.49242	0.5538	0.	583.631	1088.280	518.003	0.	0.768
4	0.485	0.54321	0.5576	0.	602.866	955.967	368.789	0.	0.982
5	0.463	0.52342	0.4388	0.	651.112	805.389	232.712	0.	1.165
RADIAL POSITION	ADIABATIC EFFICIENCY	PCLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	FIXED INSTRUMENTATION	PRESSURE RATIO	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	
1	0.7699	0.7879	1.789	1.235	L.E. CHECK WEIGHT FLOW/N0Z.	= 1.7700	= 39.413	= 0.	
2	0.8803	0.9899	1.808	1.210	T.E. CHECK WEIGHT FLOW/N0Z.	= 0.8811	= 39.441	= 0.	
3	0.7895	0.9095	1.743	1.218		= 0.8903			
4	0.9095	0.9168	1.822	1.206		= 225.50			
5	0.8731	0.8825	1.731	1.195		= 0.98178			
PERCENT DESIGN SPEED									

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0419	0.7834	0.1866	1.758	1.223
2	0.0206	0.8966	0.0923	1.801	1.204
3	0.0286	0.8658	0.1303	1.756	1.201
4	0.0987	0.9654	0.0375	1.804	1.190
5	0.0218	0.9257	0.0993	1.718	1.181

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

POINT NUMBER 16 READING NUMBER 16 DATE 4/13/1967

RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT SURF	INLET REL MACH NO.	INLET REL VFLCITY	ROTOR SPN AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
1	61.877	2.977	-0.083	1.4115	1514.756	1335.004	715.718	0.667	713.512
2	59.047	3.587	-0.853	1.3193	1410.586	1219.655	725.594	0.679	725.483
3	56.738	4.488	-1.222	1.2192	1303.654	1068.452	717.487	0.671	713.939
4	54.694	4.984	-1.586	1.1019	1160.791	956.118	692.897	0.647	677.120
5	56.535	4.935	-2.345	0.9257	1002.721	805.516	597.155	0.551	552.888
RADIAL POSITION	RFL. FIXIT FLOW ANG.	REL. DEV. ANG. T.E.	RFL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELCITY	ROTOR SPD AT EXIT	EXIT ABS VFLCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	51.105	1.665	10.772	0.8079	967.778	1320.343	832.341	0.695	607.076
2	47.630	2.900	11.417	0.7645	901.838	1210.346	815.726	0.692	607.754
3	43.577	7.407	13.161	0.6270	740.991	1101.808	798.928	0.676	536.425
4	39.318	7.868	23.376	0.6343	736.693	991.811	878.047	0.756	625.917
5	21.470	15.890	33.866	0.5845	673.410	883.964	897.584	0.779	611.024
RADIAL POSITION	DIFFUSION ST. PRESS	CH1 RISE COEFF	INLET ABS TANG. VFL	INLET ABS TANG. VFL	INLET ABS TANG. VFL	INLET REL TANG. VFL	INLET REL TANG. VFL	INLET REL TANG. VFL	AXIAL VEL. RATIO
1	0.498	0.36929	0.4875	0.	567.846	1335.004	752.497	0.851	
2	0.490	0.46039	0.5507	0.	544.074	1209.655	666.272	0.838	
3	0.570	0.53107	0.5912	0.	591.392	1088.452	510.416	0.751	
4	0.518	0.58968	0.6018	0.	610.973	956.118	380.839	0.924	
5	0.485	0.59943	0.5131	0.	641.184	805.516	242.780	1.105	
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.			
1	0.7644	0.7842	1.870	1.256	0.	43.088			
2	0.8818	0.8918	1.870	1.222	0.	41.836			
3	0.8140	0.8286	1.797	1.224	0.	47.790			
4	0.9156	0.9226	1.844	1.209	0.	44.308			
5	0.8837	0.8925	1.753	1.197	0.	46.380			
TRAVERSE POSITION	TRAVERSE ADIABATIC EFF.	TRAVERSE POLYTROPIC EFF.	FIXED INSTRUMENTATION	PRESSURE RATIO					
1	1.833	1.8429	L.E. CHECK WEIGHT FLOW	ADIABATIC EFF.	=	1.8150			
2	1.8557	1.8557	T.E. CHECK WEIGHT FLOW	POLYTROPIC EFF.	=	0.8870			
3	1.930	1.930	L.E. CHECK WEIGHT FLOW/NCZ	NOZZLE WEIGHT FLOW	=	0.8960			
4	1.950	1.950	T.E. CHECK WEIGHT FLOW	WEIGHT FLOW	=	223.67			
	= 100								
									0.98948
									1.01073
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1	0.0451	0.7844	0.1959	1.821	1.238				
2	0.0201	0.9043	0.0892	1.857	1.214				
3	0.0264	0.8797	0.1201	1.803	1.209				
4	0.0080	0.9886	0.0346	1.832	1.195				
5	0.0187	0.9360	0.0861	1.740	1.183				

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS						
	POINT NUMBER	READING NUMBER	17	DATE	4/13/1967	
RADIAL POSITION	RFL. INLET FLOW ANG.	INCID. ANG MN. CMBR. LN.	INLET REL SLCT. SURF	INLET RFL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY
1	60.594	1.694	-1.366	1.2815	1.202.279	679.715
2	57.922	2.462	-1.978	1.1959	1.285.738	682.896
3	55.981	3.731	-1.979	1.1010	1.194.488	664.938
4	54.076	4.366	-2.204	0.9935	1.071.904	638.397
5	54.655	4.055	-3.225	0.8391	913.804	555.686
RADIAL POSITION	RFL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	RFL. TURN	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ABS VELOCITY
1	55.085	5.645	5.509	1.0996	1.224.395	726.143
2	52.606	7.876	5.316	0.9690	1.096.041	697.585
3	48.707	12.537	7.274	0.8305	937.638	683.017
4	32.603	9.153	21.472	0.8311	925.831	876.667
5	14.782	9.002	39.973	0.8532	912.830	1065.197
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ARS TANG. VFL	EXIT ARS TANG. VFL	INLET REL TANG. VEL
1	0.165	0.1214	0.1844	0.	185.876	1202.279
2	0.214	0.1803	0.2333	0.	227.185	1089.392
3	0.283	0.2073	0.2404	0.	288.199	980.259
4	0.238	0.2170	0.2099	0.	396.996	861.062
5	0.130	-0.0192	-0.1517	0.	564.150	725.432
RADIAL POSITION	ADIABATIC EFFICIENCY	PCLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP RATIO	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.8294	0.834	1.228	1.073	1003.199	1.033
2	0.7630	0.770	1.242	1.084	862.829	0.966
3	0.6040	0.615	1.223	1.098	704.068	0.935
4	0.8676	0.874	1.414	1.120	496.210	1.244
5	0.9067	0.912	1.521	1.141	231.931	1.708
TRaverse	PRESSURE RATIO	* 1.3183	FIXED INSTRUMENTATION	PRESSURE RATIO	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.
TRaverse	ADIABATIC EFF.	* 0.8097			0.	14.866
TRaverse	POLYTROPIC EFF.	* 0.8170			0.	19.007
FLOW COEFFICIENT L.E.	* 0.980				0.	24.988
FLOW COEFFICIENT T.E.	* 0.950		L.F. CHECK WEIGHT FLOW/NOZ.		0.	27.100
PERCENT DESIGN SPEED	= 90		T.E. CHECK WEIGHT FLOW/NOZ.		0.	32.694
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION						
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS. RATIO	TOT. TEMP RATIO	
1	0.0166	0.7950	0.0790	1.232	1.077	
2	0.0254	0.7380	0.1252	1.251	1.089	
3	0.0360	0.6707	0.1798	1.236	1.093	
4	0.0171	0.9032	0.0753	1.409	1.114	
5	0.0181	0.9315	0.0798	1.505	1.133	

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 18 READING NUMBER 18 DATE 4/13/1967

RADIAL POSITION	RFL. INLET F10K ANG.	INCID ANG MN.CMBR,LN	INLET REL SLCT.SURF	INLET RFL MACH NO.	ROT RFL MACH NO.	INLET ABS VELOCITY AT INLET	INLET ABS MACH NO.	INLET AX. VELOCITY
1	6n.875	1.975	*1.085	1.2763	1377.009	1202.024	671.782	0.623
2	5P.050	2.1590	-1.950	1.1938	1243.673	1089.161	679.370	0.632
3	55.799	3.549	-2.161	1.1036	1186.811	980.031	669.372	0.622
4	53.524	3.814	-2.756	1.0025	1079.486	860.879	651.289	0.605
5	54.358	3.758	*3.522	0.R436	917.342	725.278	561.683	0.517
RADIAL POSITION	RFL. EXIT F10K ANG.	REL. DEV. ANGL. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROT REL. VELOCITY AT EXIT	ROT SPD MACH NO.	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	54.330	4.890	6.546	0.9108	1050.146	1188.823	699.550	0.607
2	5n.835	6.105	7.215	0.8253	947.068	1089.783	695.812	0.606
3	44.754	6.584	11.045	0.6888	794.271	992.057	711.518	0.617
4	33.192	9.742	20.332	0.6873	781.781	893.017	805.150	0.708
5	1P.862	13.082	*5.496	0.6754	760.533	795.912	911.087	0.809
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG.VEL	EXIT ABS TANG.VEL	INLET REL TANG. VFL	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.327	0.28258	0.3775	0.	336.410	1202.024	852.413	0.914
2	0.355	0.35653	0.4309	0.	355.504	1089.161	734.279	0.881
3	0.442	0.40616	0.4563	0.	433.225	980.031	558.831	0.846
4	0.395	0.43684	0.4653	0.	467.272	860.879	425.745	1.023
5	0.319	0.35909	0.2812	0.	556.057	725.278	239.856	1.350
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	TOT. TEMP	ARS. INLET FLOW ANG.	ARS. INLET FLOW ANG.	Axes, EXIT FLOW ANG.
1	0.8213	0.8305	1.457	1.139	1.139	0.	0.	28.803
2	0.8789	0.8853	1.471	1.133	1.133	0.	0.	30.726
3	0.7653	0.7774	1.459	1.149	1.149	0.	0.	37.546
4	0.9074	0.9129	1.539	1.145	1.145	0.	0.	35.678
5	0.8944	0.9027	1.563	1.192	1.192	0.	0.	38.380
TRAVERSE PRESSURE RATIO	=	1.49441	FIXED INSTRUMENTATION	PRESSURE RATIO	=	1.50100		
TRAVERSE ADIABATIC EFF.	=	0.85330	ADIABATIC EFF.	=		0.8927		
TRAVERSE POLYTROPIC EFF.	=	0.8611	POLYTROPIC EFF.	=		0.8987		
FLOW COEFFICIENT L.E.	=	0.980	NOZZLE WEIGHT FLOW	=		215.33		
FLOW COEFFICIENT T.E.	=	0.950	WEIGHT FLOW/NOZ.	=		0.98796		
PERCENT DESIGN SPEED	=	90	T.E. CHECK WEIGHT PLLOW/NOZ.			0.98295		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0258	0.8164	0.1205	1.460	1.140
2	0.0179	0.8798	0.0846	1.484	1.136
3	0.0250	0.8515	0.1164	1.473	1.137
4	0.0068	0.9669	0.0302	1.545	1.137
5	0.0109	0.9600	0.0490	1.562	1.142

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (ROTOR 2F)					
N.A.S.A. COMPRESSOR OUTPUT DATA					
BLADE ELEMENT PERFORMANCE RESULTS					
POINT NUMBER	READING NUMBER	19	19	DATE	4/13/1967
RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN CMNBR.LN	INLET REL. MACH NO.	ROTOR SPD	INLET ABS MACH NO.
1	6n.683	-1.277	1.279	1.167	675.082
2	58.025	2.565	1.1936	12.02.167	0.628
3	56.026	3.776	1.1.0999	1.089.291	0.632
4	54.251	4.541	11.03.751	980.148	680.004
5	54.882	4.282	10.49.365	663.759	660.478
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	EXIT REL. MACH NO.	ROTOR SPD	INLET ABS MACH NO.
1	53.931	4.491	6.752	0.8741	670.160
2	49.630	4.900	8.395	1.108.965	0.606
3	43.132	6.962	12.894	917.775	596.290
4	31.624	8.174	22.627	0.6734	594.450
5	18.899	13.119	35.983	0.6660	567.533
RADIAL POSITION	DIFUSION POSITION	ST. PRESS. FACTOR	CH1 RISE COEFF	INLET ARS TAN ₃ . VEL	EXIT ABS VEL
1	0.363	0.31737	0.4162	0.	1202.167
2	0.387	0.39099	0.46667	370.316	618.648
3	0.461	0.43769	0.4877	390.690	699.223
4	0.418	0.47176	0.4780	460.496	531.679
5	0.353	0.41237	0.3232	0.	497.450
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	Axes. INLET FLOW ANG.
1	0.8280	0.9378	1.512	1.152	31.842
2	0.9038	0.9094	1.531	1.144	33.314
3	0.8014	0.8127	1.517	1.158	39.056
4	0.9215	0.9263	1.574	1.150	37.746
5	0.8955	0.9020	1.572	1.154	0.
TRaverse POSITION	PRESSURE RATIO	= 1.5388	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.5420
1	TRaverse ADIABATIC EFF.	= 0.8681	ADIBATIC EFF.	= 0.9117	
2	TRaverse POLYTROPIC EFF.	= 0.8759	POLYTROPIC EFF.	= 0.9169	
3	FCLW COEFFICIENT L.E.	= 0.990	NOZZLE WEIGHT FLOW	= 214.31	
4	FCLW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW	= 0.98721	
	PERCENT DESIGN SPEED = 90		T.E. CHECK WEIGHT FLOW	= 0.99178	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIBATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0255	0.8307	0.1181	1.510	1.151
2	0.0143	0.9110	0.0661	1.539	1.144
3	0.0210	0.8859	0.0950	1.530	1.146
4	0.0031	0.9859	0.0133	1.575	1.141
5	0.0104	0.9622	0.0470	1.567	1.142

Table 6. - Listing of Blade Element Performance (continued).

NASA = TASK 1 (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 20 READING NUMBER 20 DATE 4/13/1967

RADIAL POSITION 1	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.
1	61.167	2.267	1.2711	1372.550	1201.531	663.488
2	58.313	2.853	1.1693	1279.501	1088.715	661.443
3	56.010	3.760	1.0997	1183.351	979.629	672.074
4	53.809	4.099	0.9978	1074.989	860.526	660.529
5	54.777	4.177	0.8379	911.720	724.981	629.610
RADIAL POSITION 1	RFL. EXIT FLOW ANG.	REL. TURN ANGL. T.E.	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.
2	49.040	3.600	0.8357	975.581	1188.336	716.112
3	49.157	4.427	0.7579	877.690	1089.337	714.451
4	42.530	6.360	0.6504	753.839	991.650	573.995
5	32.393	8.943	0.6288	720.274	892.651	555.109
RADIAL POSITION 1	DIFFUSION ST. PRESS FACTOR	CH1 RISE COEFF	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	AXIAL VEL. RATIO
2	0.398	0.35536	0.4561	0.	409.480	1201.531
3	0.425	0.43318	0.5091	0.	425.375	1088.715
4	0.487	0.49371	0.5432	0.	482.454	663.961
5	0.469	0.54684	0.5526	0.	508.836	509.196
RADIAL POSITION 1	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS RATIO	TOT. TEMP RATIO	ARS. INLET FLOW ANG.	ARS. EXIT FLOW ANG.
2	0.8384	0.8486	1.590	1.169	34.942	0.
3	0.9058	0.9118	1.593	1.197	36.541	0.
4	0.8468	0.8565	1.583	1.166	40.994	40.994
5	0.9282	0.9329	1.609	1.197	40.068	40.068
RADIAL POSITION 1	TRAVERSE PRESSURE RATIO	= 1.5925	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.5920	
2	TRAVERSE ADIABATIC EFF.	= 0.8900		ADIABATIC EFF.	= 0.9194	
3	FLOW POLYTROPIC EFF.	= 0.8944		POLYTROPIC EFF.	= 0.9245	
4	FLOW COEFFICIENT L.E. = r.980			NOZZLE WEIGHT FLOW	= 213.11	
5	FLOW COEFFICIENT T.E. = r.950			WEIGHT FLOW/NCZ.	WEIGHT FLOW	= 0.99102
	PERCENT DESIGN SPEED = 90		L.F. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW	= 0.98908	
			T.E. CHECK WEIGHT FLOW/NCZ.	WEIGHT FLOW		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION 1	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
2	0.0269	0.8411	0.1218	1.583	1.167
3	0.0132	0.9245	0.0605	1.602	1.156
4	0.0173	0.9122	0.0774	1.590	1.155
5	0.0035	0.9845	0.0152	1.605	1.147
	0.0116	0.9584	0.0527	1.580	1.146

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS						
	POINT NUMBER	READING NUMBER	DATE	4/13/1967		
RADIAL POSITION	REL. INLET FLOW MN.CMBR.LN.	INCID ANG SLCT.SURF	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET AX. MACH NO.
1	61.390	-0.370	1.2647	1200.169	656.638	0.607
2	58.607	3.147	1.1820	1087.081	663.711	0.616
3	56.605	4.355	1.0890	978.519	648.305	0.601
4	55.006	-1.274	0.9782	1057.341	615.745	0.570
5	55.814	5.296	0.8239	898.114	531.228	0.487
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. TURN ANGL. T.E.	EXIT REL. MACH NO.	ROTOR SPN AT EXIT	EXIT ABS VELOCITY	EXIT AX. MACH NO.
1	51.929	2.489	0.7846	922.729	1186.989	0.623
2	48.294	3.564	0.7199	837.720	1088.102	0.623
3	41.693	5.523	0.6290	730.597	990.526	0.640
4	31.526	8.070	0.6064	695.968	891.639	0.694
5	19.002	13.222	0.5665	645.732	796.292	0.746
RADIAL POSITION	DIFFUSION ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL.	EXIT ABS TANG. VEL.	INLET REL TANG. VEL.	AXIAL VEL. RATIO
1	0.449	0.38736	0.4868	0.	461.250	0.868
2	0.464	0.46469	0.5396	0.	462.696	0.840
3	0.509	0.52432	0.5745	0.	504.954	0.845
4	0.479	0.56097	0.5627	0.	529.771	0.981
5	0.442	0.55242	0.4581	0.	589.571	205.113
RADIAL POSITION	POLYTROPIC EFFICIENCY	TOT. PRESS	TOT. TEMP	ABS. EXIT FLOW ANG.		
1	0.8300	0.8417	1.658	1.188	0.	39.056
2	0.9099	0.9160	1.645	1.168	0.	39.699
3	0.8700	0.8786	1.631	1.173	0.	42.809
4	0.9231	0.9375	1.632	1.161	0.	41.918
5	0.9085	0.9145	1.611	1.161	0.	44.708
TRAVERSE POSITION	PRESSURE RATIO	FIXED INSTRUMENTATION	PRESSURE RATIO AT DIABATIC EFF.	ABS. INLET FLOW ANG.		
1	1.6375			0.		
2	1.6847			0.		
3	1.6925			0.		
4	1.6980			0.		
5	1.6950			0.		
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION						
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO	
1	0.0294	0.8419	0.1300	1.640	1.180	
2	0.0128	0.9319	0.0577	1.648	1.165	
3	0.0152	0.9273	0.0672	1.628	1.161	
4	0.0024	0.9899	0.0004	1.626	1.151	
5	0.0105	0.9639	0.0474	1.592	1.147	

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS

	POINT NUMBER	HEADING NUMBER	DATE
RADIAL POSITION 1	REL. INLET FLOW ANG. MACH CMBR.LN 3.534	INCID ANG SUCT.SURF 0.474	INLET REL. MACH NO. 1.2487
2	59.361	-0.539	1.356.452
3	57.267	5.017	1.1720
4	55.335	5.625	1.0800
5	56.501	5.901	0.9750
RADIAL POSITION 1	REL. EXIT FLOW ANG. 21.426	REL. DEV. ANG. T.E. 1.988	INLET REL. MACH NO. 0.7203
2	47.870	3.140	1.265.555
3	41.836	5.668	1.0800
4	32.379	8.929	1.166.395
5	19.184	13.404	0.9750
RADIAL POSITION 1	DIFFUSION RISE COEF 0.514	SIT. PRESS RISE COEF 0.40709	INLET ABS TANG. VEL 0.
2	0.525	0.48526	0.50/5
3	0.560	0.55347	0.5587
4	0.532	0.60759	0.5981
5	0.504	0.61414	0.5170
RADIAL POSITION 1	ADIABATIC EFFICIENCY 0.8452	POLYTROPIC EFFICIENCY 0.8565	TOT. PRESS RATIO 1.715
2	0.9039	0.9107	1.688
3	0.8859	0.88938	1.666
4	0.9438	0.9476	1.649
5	0.9371	0.9412	1.624
TRAVERSE POSITION 1	PRESSURE RATIO TRAVERSE ADIABATIC EFF. = 0.9053	1.6721 TOT. PRESS LOSS PARAM	FIXED INSTRUMENTATION ADIBATIC COEFF. = 0.9026
2	TRAVERSE POLYTROPIC EFF. = 0.9080	0.8205 0.9108	PRESSURE RATIO ADIABATIC EFF. = 0.9167
3	FLOW COEFFICIENT L.E. = 0.980	0.9246 0.9279	POLYTROPIC EFF. = 0.9225
4	FLOW COEFFICIENT T.E. = 0.95U	0.9957 0.9945	NOZZLE WEIGHT FLOW = 204.67
5	PERCENT DESIGN SPEED = 90	0.9846 0.0046	WEIGHT FLOW = 0.99596 WEIGHT FLOW = 0.9020
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION			
RADIAL POSITION 1	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT
2	0.0363 0.0181	0.8205 0.9108	0.1588 0.0808
3	0.0165	0.9246	1.682 1.669
4	0.0010	0.9957	1.660 1.650
5	0.0046	0.9846	1.616 1.149
TOT. TEMP RATIO			
37			

Table 6. - Listing of Blade Element Performance (continued)

NASA - TASK I (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

	POINT NUMBER	READING NUMBER	36	DATE	4/14/1967
RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG SUCT. SURF	INLET REL MACH NO.	INLET REL VELOCITY	INLET ABS MACH NO.
1	MN.CMBR.LN	-0.106	1.26/6	1467.258	787.382
2	61.854	-0.488	1.45/8	1544.465	786.016
3	59.412	-0.571	1.3398	1422.232	0.725
4	57.389	-0.939	1.2098	1287.230	769.190
5	55.341	-1.579	1.0123	1091.070	743.439
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT INLET
1	51.716	2.276	10.138	0.9195	1099.497
2	48.121	3.391	11.290	0.8451	998.841
3	45.209	9.039	12.179	0.6378	758.249
4	23.898	0.448	31.443	0.6757	1210.961
5	14.723	8.943	41.577	0.6993	783.798
RADIAL POSITION	DIFUSION FACTOR	ST. PRESS RISE COEFF	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL
1	0.469	0.28658	0.4170	0.	1467.258
2	0.480	0.36442	0.4702	0.	862.244
3	0.611	0.41597	0.4924	0.	586.566
4	0.556	0.42891	0.4572	0.	673.210
5	0.442	0.43953	0.3324	0.	774.524
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP	INLET REL FLOW ANG.
1	0.7341	0.7568	0.7568	1.896	0.
2	0.8160	0.8319	0.8319	1.911	40.870
3	0.7150	0.7374	0.7374	1.798	41.338
4	0.8339	0.8493	0.8493	2.004	51.587
5	0.8732	0.8846	0.8846	1.96J	47.403
TRaverse POSITION	PRESSURE RATIO =	1.9144	FIXED INSTRUMENTATION	PRESSURE RATIO =	ABS. INLET FLOW ANG. =
1	TRAVERSE ADIABATIC EFF. =	0.7909	ADIBATIC EFF. =	1.8750	0.8245
2	TRAVERSE POLYTROPIC EFF. =	0.8091	POLYTROPIC EFF. =	0.8393	0.8393
3	FLOW COEFFICIENT L.E. =	0.980	NOZZLE WEIGHT FLOW =	234.75	234.75
4	FLOW COEFFICIENT T.E. =	0.950	WEIGHT FLOW/NOZ. WEIGHT FLOW =	0.98556	0.98556
5	PERCENT DESIGN SPEED = 110	L.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW =	T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW =	1.02151	1.02151

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIBATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0518	0.7398	0.2278	1.847	1.259
2	0.0338	0.8364	0.1512	1.909	1.243
3	0.0453	0.7813	0.2121	1.797	1.233
4	0.0406	0.8526	0.1640	1.878	1.231
5	0.0189	0.9411	0.0833	1.943	1.222

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2t)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

		POINT NUMBER	READING NUMBER	DATE
RADIAL POSITION 1	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INLET SUCT.SURF MACH NO.	INLET REL VELOCITY AT INLET
2	61.836	-0.124	1.5679	1665.224
2	59.458	-0.442	1.4557	1543.494
3	57.663	-0.297	1.5346	1417.659
4	56.295	0.015	1.1921	1272.119
5	56.696	-1.184	1.0063	1085.386
RADIAL POSITION 1	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	INLET REL. MACH NO.
2	50.962	1.522	10.873	0.8766
2	47.081	2.351	12.377	0.8136
3	44.767	8.597	12.896	0.6186
4	22.283	-1.167	34.011	0.6585
5	16.206	10.426	40.490	0.6648
RADIAL POSITION 1	DIFFUSION FACTOR	ST. PRESS RISE COEF F	CH1	INLET ABS TANG. VEL
2	0.504	0.30430	0.4369	0.
2	0.509	0.37990	0.4860	0.
3	0.628	0.43989	0.5155	0.
4	0.572	0.43273	0.4579	0.
5	0.469	0.47128	0.3925	0.
RADIAL POSITION 1	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	T.C.T. TEMP
2	0.7199	0.7450	1.962	1.296
3	0.8101	0.8273	1.970	1.264
3	0.7266	0.7492	1.857	1.266
4	0.8421	0.8572	2.054	1.271
5	0.8742	0.8855	1.967	1.244
RADIAL POSITION 1	TRAVERSE PRESSURE RATIO	= 1.9651	FIXED INSTRUMENTATION	PRESSUR SURF RATIO
2	TRAVERSE ADIABATIC EFF.	= 0.7881		= 1.9210
2	TRAVERSE POLYTROPIC EFF.	= 0.8071		= 0.8285
3	FLOW COEFFICIENT L.E.	= 0.980		= 0.8435
4	FLOW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW/Noz. WEIGHT FLOW	= 233.35
PERCENT DESIGN SPEED	= 110	T.E. CHECK WEIGHT FLOW/Noz. WEIGHT FLOW	= 0.98546	
				= 1.02040
RADIAL POSITION 1	TOT. PRESS LOSS PARAM	ADIAVATRIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO
2	0.0532	0.7483	0.2302	1.920
2	0.0340	0.8440	0.1491	1.966
3	0.0451	0.7909	0.2096	1.845
4	0.0424	0.8529	0.1696	1.904
5	0.0193	0.9403	0.0859	1.957

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIAVATRIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0532	0.7483	0.2302	1.920	1.274
2	0.0340	0.8440	0.1491	1.966	1.253
3	0.0451	0.7909	0.2096	1.845	1.242
4	0.0424	0.8529	0.1696	1.904	1.237
5	0.0193	0.9403	0.0859	1.957	1.225

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK 1 (RCTOK 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
POINT NUMBER		BLADE ELEMENT PERFORMANCE RESULTS		HEADNG NUMBER		38		DATE	
17				38				4/14/1967	
REL. INLET FLOW ANG., RADIAL POSITION	REL. EXIT FLOW ANG., RADIAL POSITION	INCID ANG MN.CMBR.LN	INCID ANG SUCT. SURF	INLET REL. MACH NO.	INLET REL. MACH NO.	ROTOR SPD AT INLET	INLET ARS MACH NO.	INLET ARS MACH NO.	INLET A.S. VELOCITY
1 62.203 2 59.543 3 57.512 4 55.376 5 56.309	1 50.478 2 47.013 3 45.151 4 24.319 5 18.046	0.243 -0.357 -0.448 -0.904 -1.571	3.303 4.083 5.262 5.666 5.739	1.2604 1.4942 1.5374 1.2094 1.0123	1.660.592 1.543.124 1.420.956 1.287.317 1.091.491	1467.976 1.330.143 1196.867 1051.352 885.749	776.2P0 782.275 765.915 742.854 637.809	0.729 0.737 0.721 0.698 0.592	7/3.587 782.155 762.128 725.940 590.529
REL. INLET FLOW ANG., RADIAL POSITION	REL. EXIT FLOW ANG., RADIAL POSITION	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT A.R.S. MACH NO.	EXIT A.R.S. MACH NO.	INLET A.S. VELOCITY
1 47.013 2 45.151 3 24.319 4 18.046	1 50.478 2 47.013 3 45.151 4 24.319 5 18.046	1.038 2.283 8.981 0.869 12.260	11.725 12.530 12.362 31.057 36.269	0.8612 0.7996 0.6691 0.6430 0.6423	1040.374 951.679 728.544 751.214 741.638	1451.855 1330.902 1211.553 1090.600 972.011	928.587 907.733 864.828 1040.739 1029.264	0.769 0.763 0.723 0.891 0.891	661.415 648.873 513.451 680.311 687.756
REL. INLET FLOW ANG., RADIAL POSITION	ST. PRESS RISE COEFF FACTOR	CH1	INLET ABS TANG. VEL	EXIT A.R.S. TANG. VEL	INLET REL VEL	INLET REL VEL	INLET REL VEL	INLET REL VEL	AXIAL VEL. RATIO
1 0.516 2 0.521 3 0.636 4 0.583 5 0.488	0.30839 0.39285 0.45840 0.48905 0.53309	0.4406 0.4941 0.5341 0.5165 0.4549	0. 0. 0. 0. 0.	650.126 634.753 695.393 783.158 748.018	1467.976 1330.143 1196.867 1051.352 885.749	801.729 696.150 516.160 307.442 223.993	0.855 0.830 0.674 0.937 1.165	0. 0. 0. 0. 0.	0. 0. 0. 0. 0.
ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP	FIXED INSTRUMENTATION	PRESSURE RATIO	A.R.S. INLET FLOW ANG.	A.R.S. EXIT FLOW ANG.	A.R.S. INLET FLOW ANG.	
1 0.7190 2 0.8193 3 0.7347 4 0.8443 5 0.8788	0.7448 0.8360 0.7571 0.8593 0.8898	2.000 2.005 1.882 2.069 1.971	1.305 1.268 1.270 1.274 1.244	0. 0. 0. 0. 0.	44.507 44.370 53.559 49.020 47.403	0. 0. 0. 0. 0.	0. 0. 0. 0. 0.	44.507 44.370 53.559 49.020 47.403	
TRAVERSE ADIABATIC EFF.	= 1.9895								
TRAVERSE POLYTROPIC EFF.	= 0.7916								
FLOW COEFFICIENT L.E.	= 0.980								
FLOW COEFFICIENT T.E.	= 0.950								
PERCENT DESIGN SPEED	= 110								
44	PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION								
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1 0.0557 2 0.0348 3 0.0459 4 0.0422 5 0.0194	0.7460 0.8435 0.7896 0.8512 0.9394	0.2385 0.1526 0.2146 0.1713 0.0872	1.955 1.997 1.870 1.924 1.968	1.283 1.259 1.248 1.242 1.227					

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK I (RCTR 2E)

N.A.S.A. COMPRESSION OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 18 READING NUMBER 39 DATE 4/14/1967

RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SURF	INLET REL MACH NO.	INLET REL VELOCITY	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET AX. VELOCITY
1	60.192	1.292	-1.768	0.98/4	1077.536	934.255	536.890	0.492
2	57.413	1.953	-2.487	0.92/24	1004.743	846.535	541.190	0.497
3	54.766	2.516	-3.194	0.8580	934.097	761.715	540.674	0.497
4	52.027	2.317	-4.253	0.7866	856.335	669.106	534.422	0.491
5	52.556	1.956	-5.324	0.6681	731.542	563.712	466.244	0.426
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELOCITY	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT AX. VELOCITY
1	53.919	4.479	6.273	0.82/30	949.064	923.995	581.593	0.523
2	50.682	5.952	6.731	0.76/6	858.134	847.018	573.757	0.515
3	43.732	7.562	11.034	0.63/11	710.136	771.062	585.087	0.520
4	29.801	6.351	22.226	0.64/0	719.900	694.084	711.440	0.639
5	15.361	9.581	37.194	0.64/11	708.626	618.611	811.465	0.734
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET ABS TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.173	0.13682	0.1850	0.	157.624	157.624	766.371	1.443
2	0.207	0.20118	0.2348	0.	183.138	846.535	663.880	1.005
3	0.331	0.24474	0.2622	0.	280.502	761.715	490.559	0.953
4	0.268	0.28485	0.2695	0.	338.319	669.106	355.765	1.189
5	0.177	0.14857	0.0416	0.	435.656	563.712	182.955	1.543
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP	MOMEN RISE / MEAS. T. RISE	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	
1	0.8416	0.8446	1.142	1.046	1.0167	0.	15.762	
2	0.8495	0.8527	1.161	1.052	0.9697	0.	18.615	
3	0.6252	0.6334	1.170	1.073	0.9512	0.	28.681	
4	0.9224	0.9251	1.271	1.079	0.9641	0.	28.574	
5	0.9424	0.9447	1.329	1.090	0.9674	0.	33.192	
TRAVERSE PRESSURE RATIO	= 1.2110	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.2180				
TRAVERSE ADIABATIC EFF.	= 0.8458	ADIABATIC EFF.	= 0.9254					
TRAVERSE POLYTROPIC EFF.	= 0.8500	POLYTROPIC EFF.	= 0.9275					
FLOW COEFFICIENT L.E.	= 0.980	NOZLF WEIGHT FLOW	= 1.95.64					
FLOW COEFFICIENT T.E.	= 0.950	NOZWF WEIGHT FLOW	= 0.99082					
PERCENT DESIGN SPEED	= 70	L.E. CHECK WEIGHT FLOW/NOZ.	= 0.96290					
		T.E. CHECK WEIGHT FLOW/NOZ.						
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION								
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO			
1	0.0102	0.8582	0.0470	1.148	1.047			
2	0.0089	0.8948	0.0421	1.110	1.051			
3	0.0247	0.7918	0.1126	1.187	1.063			
4	0.0002	0.9989	0.0008	1.281	1.073			
5	-0.0038	1.0158	-0.0168	1.326	1.083			

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK I (RCTR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS									
	POINT NUMBER	19	READING NUMBER	40	DATE	4/14/1967			
RADIAL POSITION	REFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SURF	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ARS VELOCITY	INLET ARS MACH NO.	INLET ARS MACH NO.	INLET AX. VELOCITY
1	61.160	2.260	-0.800	0.9720	1068.741	935.509	516.750	0.471	515.157
2	58.420	2.960	-1.480	0.9103	995.067	847.671	521.165	0.477	521.086
3	56.236	3.986	-1.724	0.8403	918.894	762.737	512.456	0.469	509.917
4	54.153	4.443	-2.127	0.7612	833.224	670.003	495.336	0.453	484.057
5	54.795	4.199	-3.081	0.6450	709.646	564.468	430.086	0.391	398.204
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ARS VELOCITY	EXIT ARS MACH NO.	EXIT ARS MACH NO.	EXIT AX. VELOCITY
1	52.928	3.488	8.232	0.7463	846.952	925.235	569.221	0.502	510.104
2	49.077	4.347	9.343	0.6732	760.841	848.155	568.403	0.503	498.378
3	41.998	5.828	14.238	0.5921	669.870	772.096	594.353	0.525	497.449
4	30.103	6.653	24.050	0.5566	626.307	695.016	664.155	0.590	538.803
5	15.727	9.947	39.072	0.5378	601.812	619.441	740.879	0.662	564.626
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEF	CH1	INLET ABS TANG. VEL.	EXIT ARS TANG. VEL.	INLET RFL TANG. VFL	EXIT REL TANG. VEL.	AXIAL VEL. RATIO	
1	0.293	0.27806	0.3415	0.	250.069	935.509	675.166	0.990	
2	0.327	0.34412	0.36842	0.	273.281	847.671	574.874	0.956	
3	0.379	0.39476	0.4180	0.	324.222	762.737	447.874	0.976	
4	0.374	0.42009	0.4647	0.	382.644	670.003	312.372	1.113	
5	0.311	0.34233	0.2361	0.	460.440	564.468	159.001	1.418	
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP					
1	0.8683	0.8726	1.258	1.078					
2	0.9399	0.9419	1.260	1.074					
3	0.8894	0.8932	1.280	1.082					
4	0.9473	0.9493	1.316	1.086					
5	0.9524	0.9543	1.341	1.092					
TRaverse	PRESSURE RATIO	= 1.2889	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.2910				
TRaverse	ADIABATIC EFF.	= 0.9186		ADIABATIC EFF.	= 0.9634				
TRaverse	POLYTROPIC EFF.	= 0.9215		POLYTROPIC EFF.	= 0.9647				
FLOW COEFFICIENT L.E.	= 0.980			NOZZLE WEIGHT FLOW	= 178.53				
FLOW COEFFICIENT T.E.	= 0.950		L.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	= 0.98294				
PERCENT DESIGN SPEED	= 70		T.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	= 0.96265				
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO					
1	0.0106	0.9092	0.0479	1.262					
2	0.0049	0.9613	0.0224	1.272					
3	0.0087	0.9436	0.0384	1.281					
4	0.0008	0.9960	0.0033	1.314					
5	-0.0003	1.0013	-0.0016	1.339					
				0.					

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

POINT NUMBER 20 READING NUMBER 41 DATE 4/14/1967

RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INLET REL SUCT.SURF	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.
1	62.051	3.151	0.091	0.9640	1058.292	497.198	495.665
2	59.370	3.910	-0.530	0.8980	983.806	846.507	501.222
3	57.101	4.851	-0.859	0.8295	908.510	761.690	492.746
4	54.787	5.077	-1.493	0.7529	825.355	669.084	483.224
5	55.516	4.916	-2.364	0.6358	701.877	563.693	418.188
						0.379	387.188
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	EXIT REL. MACH NO.	EXIT REL. VELOCITY	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.
1	53.011	3.571	9.040	0.7115	811.066	923.965	561.632
2	49.013	4.283	10.357	0.6422	729.257	846.990	562.772
3	42.740	6.570	14.361	0.2630	639.741	771.036	578.562
4	31.113	7.663	23.673	0.5207	588.848	694.061	639.065
5	16.815	11.035	38.700	0.5049	5668.387	618.591	712.308
						0.633	530.465
RADIAL POSITION	DIFFUSION FACTOR RISE COEF F	ST. PRESS CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	AXIAL VEL. RATIO
1	0.329	0.31208	0.3773	0.	276.695	934.225	0.984
2	0.360	0.386079	0.4221	0.	296.514	846.507	0.954
3	0.409	0.43577	0.4284	0.	337.184	761.690	433.852
4	0.417	0.48056	0.4641	0.	391.451	669.084	302.610
5	0.350	0.42850	0.3267	0.	458.279	563.693	160.312
							1.370
RADIAL POSITION	ADIABATIC EFFICIENCY	TOT. PRESS	TCT. TEMP RATIO	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	ARS. EXIT FLOW ANG.	
1	0.8674	0.8720	1.287	1.086	0.	29.576	
2	0.9289	0.9315	1.295	1.082	0.	31.796	
3	0.8740	0.8786	1.295	1.088	0.	35.685	
4	0.9294	0.9322	1.325	1.090	0.	37.981	
5	0.9611	0.9627	1.345	1.092	0.	40.824	
TRAVERSE PRESSURE RATIO	= 1.3068	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.3110			
TRAVERSE ADIABATIC EFF.	= 0.9096		ADIABATIC EFF.	= 0.9646			
TRAVERSE POLYTROPIC EFF.	= 0.9150		POLYTROPIC EFF.	= 0.9660			
C. LOW COEFFICIENT L.E.	= 0.980		NOZZLE WEIGHT FLOW	= 172.54			
FLOW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	= 0.98906			
PERCENT DESIGN SPEED	= 70	T.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	= 0.95864			
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION							
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO		
1	0.0118	0.9095	0.0532	1.292	1.084		
2	0.0058	0.9590	0.0263	1.299	1.081		
3	0.0078	0.9519	0.0352	1.301	1.082		
4	-0.0001	1.0006	-0.0005	1.326	1.084		
5	-0.0011	1.0039	-0.0048	1.344	1.088		

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2t)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS
POINT NUMBER 21 READING NUMBER 42 DATE 4/14/1967

RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SUH	INLET REL MACH NO.	INLET REL VELOCITY AT INLET	ROTOR SPD	INLET ARS VELOCITY AT INLET	INLET ARS MACH NO.	INLET ARS MACH NO.
1	62.48E	3.588	0.528	0.9590	1953.059	933.357	487.626	0.444	486.123
2	59.89E	4.38	-0.062	0.8915	97/.593	845.720	490.352	0.447	490.277
3	57.89E	5.644	-0.066	0.8199	899.640	760.982	479.853	0.437	477.481
4	55.87E	6.162	-0.408	0.7407	813.302	668.462	463.620	0.422	453.064
5	56.56E	5.968	-1.312	0.6265	691.672	563.170	401.560	0.364	371.793
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ARS VELOCITY AT EXIT	ROTOR SPD AT EXIT	EXIT ARS MACH NO.	EXIT ARS MACH NO.
1	52.93E	3.498	9.221	0.6929	/91.352	923.106	559.963	0.490	476.514
2	48.73E	4.007	11.162	0.6194	702.257	846.203	562.371	0.494	495.122
3	42.34E	6.176	15.547	0.5424	617.123	770.320	578.161	0.508	455.766
4	30.99E	7.549	24.873	0.2088	575.778	693.417	635.103	0.561	490.852
5	15.80E	10.023	40.765	0.4880	549.411	618.016	709.598	0.630	515.240
RADIAL POSITION	ST. PRESS RISE COEF F	CH1	INLET ABS TANG. VEL	EXIT ARS TANG. VFL	INLET RFL TANG. VFL	INLET REL TANG. VEL	INLET RFL TANG. VEL	AXIAL VFL RATIO	AXIAL VFL RATIO
1	0.350	0.33186	0.3980	0.	292.184	933.357	630.922	0.546	0.546
2	0.387	0.39922	0.4435	0.	316.079	457.720	530.124	0.549	0.549
3	0.434	0.44845	0.4700	0.	354.932	760.982	415.388	0.555	0.555
4	0.427	0.48313	0.4642	0.	398.506	668.462	294.910	1.042	1.042
5	0.373	0.43363	0.5216	0.	472.173	563.170	145.843	1.346	1.346
RADIAL POSITION	ADIABATIC POLYTROPIC EFFICIENCY	TOT. PPRESS	TCT. TEMP RATIO	ARS. INLET FLOW ANG.	ARS. EXIT FLOW ANG.	ARS. INLET FLOW ANG.	ARS. EXIT FLOW ANG.		
1	0.86668	0.8717	1.305	1.091	1.	31.515	0.		
2	0.9114	0.9147	1.308	1.088	0.	34.199	0.		
3	0.8867	0.8910	1.306	1.090	0.	37.910	0.		
4	0.9390	0.9415	1.329	1.090	0.	59.073	0.		
5	0.9498	0.9519	1.349	1.094	0.	42.500	0.		
TRAVERSE PRESSURE RATIO	= 1.3177	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.3190					
TRAVERSE ADIABATIC EFF.	= 0.9079		ADIABATIC EFF.	= 0.9635					
TRAVERSE POLYTROPIC EFF.	= 0.9114		POLYTROPIC EFF.	= 0.9649					
FLOW COEFFICIENT L.E.	= 0.980		NOZZLE WEIGHT FLOW	= 169.39					
FLOW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 0.98380						
PERCENT DESIGN SPEED	= 70	T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 0.95848						
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1	0.0140	0.8983	0.0632	1.306	1.088				
2	0.0052	0.9645	0.0237	1.312	1.084				
3	0.0073	0.9571	0.0324	1.309	1.084				
4	-0.0006	1.0026	-0.0024	1.331	1.085				
5	-0.0000	1.0001	-0.0000	1.346	1.089				

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK 1 (RCTOR 2b)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS
POINT NUMBER 22 READING NUMBER 43 DATE 4/14/1967

RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SURF	INLET REL MACH NO.	INLET SPD AT INLET VELOCITY	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
1	6.3.949	5.049	1.989	0.9443	1039.322	933.174	457.577	0.416
2	61.342	5.882	1.442	0.8781	963.628	845.533	462.185	462.115
3	59.225	6.975	1.265	0.8087	886.683	760.833	455.346	453.094
4	56.988	7.278	0.708	0.7318	802.557	668.331	444.333	434.216
5	57.966	7.366	0.086	0.6169	679.577	563.059	380.511	352.304
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. MACH NO.	EXIT ABS VELOCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	52.545	3.105	11.405	0.6474	742.418	922.926	562.232	0.490
2	48.955	4.225	12.387	0.5829	665.326	846.038	556.233	0.487
3	43.900	7.730	15.325	0.5036	574.728	770.169	556.810	413.613
4	31.883	8.433	25.163	0.4740	536.895	693.281	614.662	453.434
5	15.987	10.207	41.979	0.4587	516.597	617.895	690.852	0.613
RADIAL POSITION	DIFFUSION RISE COEF	ST. PRESS RISE COEF	CH1	INLET ABS TANG. VFL	EXIT ABS TANG. VFL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VFL. RATIO
1	0.403	0.36670	0.4293	0.	334.107	933.174	588.819	0.589
2	0.429	0.43119	0.4747	0.	344.262	845.555	501.776	0.545
3	0.480	0.48517	0.6052	0.	372.146	760.833	398.023	0.913
4	0.472	0.53731	0.2125	0.	411.227	668.331	282.054	1.044
5	0.412	0.50634	0.3894	0.	479.206	563.059	138.689	1.374
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP	TCT. TEMP	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	
1	0.8734	0.8736	1.341	1.100	1.100	0.	36.526	
2	0.9049	0.9088	1.334	1.095	1.095	0.	38.238	
3	0.8529	0.8586	1.318	1.097	1.097	0.	41.979	
4	0.9330	0.9357	1.342	1.094	1.094	0.	42.205	
5	0.9452	0.9476	1.363	1.098	1.098	0.	44.710	
TRAVERSE POSITION	TRAVERSE PRESSURE RATIO	FIXED INSTRUMENTATION	PRESSURE RATIO	ADIABATIC EFF.	ADIABATIC EFF.			1.3410
1	= 1.3393		=	=	=			0.9461
2	= 0.8990							0.9483
3	= 0.9032							161.84
4	= 0.986							0.98697
5	= 0.950	L.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW	=	=			0.95356
		T.E. CHECK WEIGHT FLOW/NOZ.	WEIGHT FLOW					
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP			
1	0.0197	0.8746	0.0885	1.338	1.099			
2	0.0097	0.9404	0.0441	1.337	1.092			
3	0.0111	0.9381	0.0510	1.327	1.090			
4	0.0008	0.9966	0.0033	1.348	1.089			
5	0.0000	0.9999	0.0001	1.359	1.092			
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION								

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
BLADE ELEMENT PERFORMANCE RESULTS			POINT NUMBER 23 READING NUMBER 44			DATE 4/14/1967			
RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SURF	INLET REL MACH NO.	INLET REL VELOCITY	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS VELOCITY	INLET AX. VELOCITY
1	65.311	6.411	3.351	0.9324	1030.238	935.554	431.427	0.390	430.097
2	62.829	7.369	2.929	0.8625	952.895	847.711	435.194	0.395	435.128
3	60.985	8.735	3.025	0.7933	873.264	762.773	425.167	0.386	423.065
4	58.988	9.278	2.708	0.7141	786.664	670.036	412.180	0.374	402.795
5	59.597	8.997	1.717	0.6048	668.313	564.495	357.753	0.324	331.233
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELOCITY	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS VELOCITY	EXIT AX. VELOCITY
1	52.677	3.237	12.634	0.6098	704.016	925.280	562.736	0.487	426.471
2	49.235	4.505	13.593	0.2523	633.652	848.195	553.913	0.483	413.738
3	44.219	8.049	16.767	0.4557	522.174	772.133	553.973	0.483	373.569
4	31.105	7.659	27.878	0.4498	511.968	695.049	616.043	0.541	435.935
5	15.412	9.632	44.184	0.4413	498.377	613.471	687.159	0.608	468.263
RADIAL POSITION	DIFFUSION RISE COEF.F FACTOR	ST. PRESS RISE COEF.F	CHI	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET RFL TANG. VFL	EXIT RFL TANG. VFL	INLET RFL TANG. VFL	AXIAL VEL. RATIO
1	0.446	0.37363	0.4399	0.	365.930	935.554	559.349	0.992	0.992
2	0.464	0.43752	0.4799	0.	368.277	847.711	479.319	0.551	0.551
3	0.545	0.48685	0.5049	0.	408.226	762.773	363.907	0.884	0.884
4	0.500	0.54324	0.2178	0.	431.978	670.036	263.071	1.082	1.082
5	0.434	0.53350	0.4096	0.	490.380	564.495	129.091	1.414	1.414
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP RATIO	TCT. TEMP RATIO	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	ABS. INLET FLOW ANG.	ADIABATIC EFF. = 0.9061
1	0.8267	0.8340	1.357	1.111	1.111	0.	40.631	40.631	POLYTROPIC EFF. = 0.9100
2	0.8594	0.8652	1.344	1.103	1.103	0.	41.673	41.673	NOZZLE WEIGHT FLOW = 153.93
3	0.8192	0.8263	1.324	1.102	1.102	0.	47.508	47.508	WEIGHT FLOW = 0.97904
4	0.9014	0.9055	1.352	1.100	1.100	0.	44.739	44.739	WEIGHT FLOW = 0.94721
5	0.9575	0.9593	1.373	1.099	1.099	0.	46.322	46.322	WEIGHT FLOW = 0.94721
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1	0.0319	0.8165	0.1436	1.352	1.110				
2	0.0175	0.9000	0.0801	1.346	1.098				
3	0.0196	0.8992	0.0901	1.335	1.096				
4	0.0081	0.9666	0.0350	1.354	1.094				
5	0.0069	0.9766	0.0306	1.367	1.095				

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK 1 (RCTR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
BLADE ELEMENT PERFORMANCE RESULTS									
		POINT NUMBER		READING NUMBER		45		DATE	
RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	SUCT.SURF	INLET REL MACH NO.	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
1	60.661	1.761	-1.299	0.6936	765.504	666.819	375.964	0.341	374.805
2	57.465	2.005	-2.435	0.6507	716.711	604.209	385.195	0.350	385.436
3	54.682	2.432	-3.278	0.6067	667.409	543.669	387.115	0.352	385.601
4	51.876	2.166	-4.404	0.5568	612.499	477.570	383.513	0.349	374.781
5	52.503	1.903	-5.377	0.4737	522.538	402.346	333.413	0.302	308.697
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	53.115	3.975	7.245	0.6090	678.647	659.496	421.133	0.378	404.131
2	49.021	4.291	8.444	0.5538	616.870	604.554	427.707	0.384	404.525
3	42.295	6.125	12.387	0.4932	349.737	550.341	445.197	0.399	406.330
4	29.120	5.670	22.576	0.4729	525.718	495.399	519.389	0.467	426.649
5	13.970	8.190	38.533	0.4703	520.330	441.530	598.011	0.541	491.964
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF F	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO	AXIAL VEL.
1	0.168	0.15714	0.1899	0.	0.	115.032	666.819	544.464	1.078
2	0.204	0.22041	0.23/8	0.	0.	138.855	604.209	465.699	1.050
3	0.259	0.26924	0.2709	0.	0.	180.673	543.669	369.667	1.055
4	0.250	0.28414	0.2536	0.	0.	241.023	477.570	254.376	1.218
5	0.154	0.10705	-0.0086	0.	0.	319.142	402.346	122.388	1.594
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP	FIXED INSTRUMENTATION	PRESSURE RATIO	A.DIABATIC EFF.	1.1160	
1	0.8881	0.8693	1.079	1.025	0.	15.888	0.	0.9624	
2	0.9041	0.9054	1.091	1.028	0.	18.945	0.	0.9630	
3	0.8314	0.8338	1.103	1.034	0.	23.972	0.	142.08	
4	0.9343	0.9356	1.139	1.041	0.	27.825	0.	0.9749	
5	0.9736	0.9742	1.165	1.046	0.	32.972	0.	0.96037	
TRAVERSE PRESSURE RATIO = 1.1133 TRAVERSE ADIABATIC EFF. = 0.9145 TRAVERSE POLYTROPIC EFF. = 0.9158 FLOW COEFFICIENT L.E. = 0.980 FLOW COEFFICIENT T.E. = 0.950 PERCENT DESIGN SPEED = 50									
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP	TOT. TEMP RATIO			
1	0.0058	0.9142	0.0265	1.082	1.025	1.028			
2	0.0036	0.9565	0.0166	1.096	1.028	1.033			
3	0.0085	0.9443	0.0380	1.110	1.040	1.039			
4	0.0024	0.9852	0.0103	1.140	1.044	1.044			
5	0.0009	0.9963	0.0039	1.163					

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
		POINT NUMBER		BLADE ELEMENT PERFORMANCE RESULTS		DATE			
		25		HEADING NUMBER		4/14/1967			
RADIAL POSITION	RFL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	SUCT.SURF	INLET REL MACH NO.	INLET REL MACH NO.	ROTOR SPD AT INLET	INLET ABS MACH NO.	INLET ABS MACH NO.	INLET AX. VELOCITY
1	61.693	2.793	-0.267	0.6837	756.668	665.722	359.668	0.325	358.560
2	58.506	3.046	-1.394	0.6405	707.451	603.215	369.619	0.335	369.563
3	55.993	3.743	-1.967	0.5942	656.780	542.775	368.026	0.333	366.207
4	53.631	3.921	-2.649	0.5409	597.007	476.784	359.297	0.326	351.117
5	54.100	3.500	-3.780	0.4608	509.881	401.684	314.052	0.284	290.772
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANGL. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT	EXIT AX. VELOCITY			
1	53.382	3.942	8.311	0.5813	651.414	612.255	412.255	0.368	388.220
2	48.852	4.122	9.654	0.5257	588.415	603.559	418.494	0.374	385.658
3	42.346	6.176	13.647	0.4657	521.345	549.435	433.667	0.387	385.034
4	29.318	5.868	24.313	0.4395	490.609	494.583	499.031	0.447	425.339
5	14.291	8.511	39.809	0.4367	484.803	440.803	571.436	0.514	427.760
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	INLET ABS TANG. VEL	INLET ABS TANG. VEL	INLET ABS TANG. VEL	INLET ABS TANG. VEL	AXIAL VEL. RATIO
1	0.205	0.20537	0.2415	0.	0.	136.023	665.722	522.387	1.083
2	0.248	0.26898	0.2852	0.	0.	161.987	603.215	441.572	1.044
3	0.297	0.31410	0.3160	0.	0.	198.518	542.775	350.917	1.051
4	0.296	0.32715	0.2946	0.	0.	255.717	476.784	238.866	1.211
5	0.205	0.18415	0.0654	0.	0.	324.196	401.684	116.607	1.574
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP RATIO	MOMEN RISE/ NFAS T. RISE	ABS. EXIT FLOW ANG.			
1	0.8672	0.8690	1.098	1.031	0.9220	0.9220	0.9220	0.9220	19.309
2	0.8795	0.8812	1.106	1.033	0.9423	0.9423	0.9423	0.9423	22.773
3	0.8490	0.8513	1.114	1.037	0.9508	0.9508	0.9508	0.9508	27.275
4	0.9330	0.9343	1.143	1.042	0.9770	0.9770	0.9770	0.9770	31.015
5	0.9785	0.9790	1.165	1.046	1.0076	1.0076	1.0076	1.0076	35.307
TRAVERSE POSITION	TRAVERSE PRESSURE RATIO	= 1.1233	FIXED INSTRUMENTATION	PRESSURE RATIO	= 1.1270				
1	TRAVERSE ADIABATIC EFF.	= 0.9065	ADIASTIC EFF.	ADIASTIC EFF.	= 0.9905				
2	TRAVERSE POLYTROPIC EFF.	= 0.9080		POLYTROPIC EFF.	= 0.9907				
3	FLOW COEFFICIENT L.E.	= 0.980		NOZLE WEIGHT FLOW	= 137.06				
4	FLOW COEFFICIENT T.E.	= 0.950	L.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 0.96428				
5	PERCENT DESIGN SPEED	= 50	T.E. CHECK WEIGHT FLOW	WEIGHT FLOW	= 0.94968				
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIASTIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO				
1	0.0052	0.9358	0.0239	1.101	1.030				
2	0.0015	0.9840	0.0069	1.111	1.031				
3	0.0059	0.9516	0.0265	1.120	1.035				
4	-0.0042	1.0247	-0.0179	1.146	1.039				
5	-0.0079	1.0325	-0.0349	1.164	1.043				

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK 1 (RCTR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
		BLADE ELEMENT PERFORMANCE RESULTS		POINT NUMBER 26		READING NUMBER 47		DATE 4/14/1967	
RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID REL SUCT.SURF	INLET REL MACH NO.	INLET REL VELOCITY	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
1	62.870	3.970	0.910	0.6772	750.624	667.608	343.127	0.310	342.669
2	59.774	4.314	-0.126	0.6327	700.136	604.924	352.501	0.319	352.447
3	57.185	4.935	-0.775	0.5861	648.607	544.313	352.725	0.319	350.981
4	54.764	5.054	-1.516	0.5350	589.964	478.135	345.007	0.312	337.738
5	55.234	4.634	-2.646	0.4535	503.459	402.822	302.003	0.272	2/9.615
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELOCITY	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	53.131	3.691	9.740	0.5540	622.549	605.277	407.943	0.363	373.195
2	48.964	4.234	10.810	0.5032	564.919	605.270	411.902	0.367	370.883
3	42.656	6.486	14.530	0.4452	500.152	550.992	424.922	0.378	367.557
4	30.121	6.671	24.643	0.4195	469.754	495.985	483.873	0.432	404.049
5	15.101	9.321	40.133	0.4107	458.664	442.053	550.296	0.493	431.557
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CHI	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	ROTOR SPD TANG. VEL	INLET ABS TANG. VEL	INLET ABS TANG. VEL	AXIAL VEL. RATIO
1	0.250	0.24154	0.2798	0.	0.	162.671	667.608	497.606	1.691
2	0.279	0.30583	0.3260	0.	0.	179.161	604.924	426.109	1.052
3	0.329	0.35491	0.3569	0.	0.	212.343	544.313	338.649	1.047
4	0.325	0.37926	0.3458	0.	0.	261.566	478.135	234.418	1.196
5	0.247	0.26499	0.1442	0.	0.	325.599	402.822	116.454	1.543
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP RATIO	FIXED INSTRUMENTATION	PRESSURE RATIO	ABS. INLET FLOW ANG.	ABS. EXIT FLOW ANG.	
1	0.8877	0.8894	1.114	1.035			0.	23.552	
2	0.9140	0.9155	1.120	1.036			0.	25.784	
3	0.8805	0.8825	1.124	1.039			0.	30.016	
4	0.9754	0.9759	1.149	1.042			0.	32.918	
5	0.9781	0.9786	1.167	1.046			0.	37.034	
	TRAVERSE PRESSURE RATIO	=	1.1331				=	1.1370	
	TRAVERSE ADIABATIC EFF.	=	0.9280				=	0.9806	
	TRAVERSE POLYTROPIC EFF.	=	0.9293				=	0.9810	
	FLOW COEFFICIENT L.E.	=	0.980				=	131.76	
	FLOW COEFFICIENT T.E.	=	0.950				=	0.96173	
	PERCENT DESIGN SPEED	=	50				=	0.95094	
	PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION								
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO			TOT. TEMP RATIO		
1	0.0065	0.9318	0.0296	1.116			1.034		
2	0.0025	0.9767	0.0116	1.124			1.035		
3	0.0062	0.9544	0.0277	1.131			1.037		
4	-0.0015	1.0080	-0.0063	1.152			1.041		
5	-0.0050	1.0195	-0.0222	1.167			1.044		

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 27 READING NUMBER 48 DATE 4/14/1967

RADIAL POSITION	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INLET REL SUFT SURF	INLET REL MACH NO.	INLET SPD AT INLET VELOCITY	INLET ABS MACH NO.	INLET AX. VELOCITY
1	63.332	4.432	1.372	0.6723	745.490	665.768	354.386
2	60.425	4.965	0.525	0.6264	693.658	603.257	342.356
3	58.056	5.806	0.096	0.5790	640.575	542.812	338.451
4	55.803	6.093	-0.477	0.5250	580.766	476.817	331.563
5	56.253	5.653	-1.627	0.4469	495.378	401.712	289.873
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	ROTOR SPD AT EXIT VELOCITY	EXIT ABS MACH NO.	EXIT AX. VELOCITY
1	53.250	3.810	10.082	0.5363	603.826	658.457	401.977
2	48.760	4.030	11.665	0.4864	546.605	603.601	408.577
3	42.858	6.688	15.198	0.4277	480.424	549.473	416.990
4	29.814	6.364	25.989	0.4024	450.569	494.618	476.761
5	14.907	9.127	41.346	0.3934	439.011	440.834	538.545
RADIAL POSITION	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.276	0.26630	0.3057	0.	175.065	665.768	360.972
2	0.305	0.33070	0.3512	0.	192.588	603.257	360.327
3	0.356	0.37803	0.3796	0.	222.935	542.812	351.910
4	0.353	0.40015	0.3651	0.	271.862	476.817	388.734
5	0.277	0.29708	0.1731	0.	330.777	401.712	110.058
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TGT. PRESS	TCT. TEMP	FIXED INSTRUMENTATION	PRESSURE RATIO	ABS. INLF T FLOW ANG.
1	0.8700	0.8721	1.122	1.038	1.038	25.873	0.
2	0.9410	0.9420	1.128	1.037	1.037	28.124	0.
3	0.8874	0.8893	1.129	1.040	1.040	32.354	0.
4	0.9660	0.9667	1.152	1.043	1.043	34.967	0.
5	0.9681	0.9688	1.167	1.047	1.047	38.663	0.
RADIAL POSITION	TRAVERSE ADIABATIC EFF.	TRAVERSE POLYTROPIC EFF.	LOSS COEFFICIENT	TOT. PRESS RATIO	ADIABATIC EFF.	POLYTROPIC EFF.	NOZZLE WEIGHT FLOW
1	= 0.9275	= 0.9288	0.0275	1.125	= 0.9952	= 0.9953	= 127.96
2	= 0.9420	= 0.9440	0.0019	1.131			
3	= 0.8893	= 0.8874	0.0173	1.136			
4	= 0.9667	= 0.9660	-0.0243	1.155			
5	= 0.9688	= 0.9681	-0.0274	1.167			
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO		
1	0.0060	0.9407	0.0275	1.125	1.036		
2	0.0004	0.9964	0.0019	1.131	1.036		
3	0.0039	0.9725	0.0173	1.136	1.038		
4	-0.0058	1.0302	-0.0243	1.155	1.041		
5	-0.0062	1.0235	-0.0274	1.167	1.044		
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION							
L.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 50	T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW	= 0.96262				

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA

BLADE ELEMENT PERFORMANCE RESULTS

POINT NUMBER 28 READING NUMBER 49 DATE 4/14/1967

	REL. INLET FLOW ANG.	INCID ANG MN.CMBR.LN	INCID ANG SUCT.SURF	INLET REL MACH NO.	INLET REL VELOCITY AT INLET	ROTOR SPD AT INLET	INLET ABS VELOCITY	INLET ABS MACH NO.
RADIAL POSITION	64.872	5.972	2.912	0.6651	738.143	667.911	314.246	313.277
1	61.978	6.518	2.078	0.6189	685.592	605.198	322.137	322.088
2	59.480	7.230	1.520	0.5718	632.953	544.559	322.621	321.026
3	57.120	7.410	0.840	0.5180	573.542	478.352	316.433	309.228
4	57.589	6.989	-0.291	0.4407	488.654	403.005	276.350	255.865
RADIAL POSITION	REL. EXIT FLOW ANG.	REL. DEV. ANG. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT REL. VELOCITY AT EXIT	ROTOR SPD AT EXIT	EXIT ABS VELOCITY	EXIT ABS MACH NO.
1	53.529	4.089	11.343	0.5121	577.993	669.576	396.106	343.274
2	49.530	4.800	12.448	0.4627	520.799	605.544	397.611	338.019
3	43.727	7.557	15.753	0.4024	452.811	551.242	405.072	0.360
4	31.393	7.943	25.727	0.3770	422.954	496.210	455.695	0.406
5	16.127	10.347	41.462	0.3663	409.582	442.253	515.028	0.461
RADIAL POSITION	DIFFUSION FACTOR	ST. PRESS RISE COEFF	CH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VEL. RATIO
1	0.314	0.30543	0.3465	0.	0.	196.181	667.911	1.049
2	0.343	0.37141	0.3924	0.	0.	209.354	605.198	396.190
3	0.399	0.42494	0.4262	0.	0.	238.474	544.559	312.768
4	0.395	0.46196	0.4253	0.	0.	277.093	478.352	219.117
5	0.328	0.39701	0.2696	0.	0.	331.354	403.005	110.899
RADIAL POSITION	ADIABATIC EFFICIENCY	POLYTROPIC EFFICIENCY	TOT. PRESS	TCT. TEMP				ABS. EXIT FLOW ANG.
1	0.8768	0.8790	1.139	1.043	0.	0.	0.	29.748
2	0.9452	0.9463	1.141	1.041	0.	0.	0.	31.772
3	0.8971	0.8990	1.140	1.043	0.	0.	0.	36.104
4	0.9689	0.9695	1.15/	1.044	0.	0.	0.	37.657
5	0.9683	0.9690	1.171	1.048	0.	0.	0.	40.824
	TRaverse Pressure Ratio =	1.1483	FIXED INSTRUMENTATION		PRESSURE RATIO =			Abs. Exit Flow Ang.
	Traverse Adiabatic Eff. =	0.9296			Adiabatic Eff. =			0.9630
	Traverse Polytropic Eff. =	0.9310			Polytropic Eff. =			0.9638
	Flow Coefficient L.E. =	0.980			Nozzle Weight Flow =			122.49
	Flow Coefficient T.E. =	0.950			L.E. Check Weight Flow/Noz. =			0.95554
	Percent Design Speed =	50			T.E. Check Weight Flow/Noz. =			0.93921

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT. TEMP RATIO
1	0.0133	0.8891	0.0610	1.139	1.043
2	0.0052	0.9602	0.0237	1.145	1.041
3	0.0084	0.9455	0.0383	1.145	1.042
4	-0.0020	1.0098	-0.0085	1.161	1.043
5	-0.0025	1.0089	-0.0110	1.170	1.046

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RCTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA									
BLADE ELEMENT PERFORMANCE RESULTS				POINT NUMBER		READING NUMBER		DATE	
RADIAL POSITION		REL. INLET FLOW ANG.	INCID ANG MACH, CMBR, LN	INLET REL MACH NO.	INLET REL VELOCITY	INLET ARS MACH NO.	INLET ABS MACH NO.	INLET AX. VELOCITY	
1	67.072	8.172	5.112	0.6507	723.692	282.674	0.254	281.802	
2	64.197	8.737	4.297	0.6036	670.521	291.809	0.263	291.854	
3	62.028	9.778	4.068	0.5548	615.686	543.16	0.261	288.461	
4	59.991	10.281	3.711	0.4994	554.229	477.128	0.254	275.570	
5	60.407	9.807	2.527	0.4242	471.572	401.974	0.222	228.292	
RADIAL POSITION		REL. EXIT FLOW ANG.	REL. DEV. ANGL. T.E.	REL. TURN ANGLE	EXIT REL. MACH NO.	EXIT ABS VELOCITY	EXIT ARS MACH NO.	EXIT AX. VELOCITY	
1	53.642	4.202	13.430	0.4576	519.680	391.364	0.345	307.817	
2	49.959	5.229	14.238	0.4207	475.779	603.995	0.344	306.079	
3	43.240	7.070	18.789	0.3522	398.034	549.832	0.355	289.755	
4	31.394	7.944	28.597	0.3453	388.857	494.940	0.394	350.124	
5	15.360	9.580	45.047	0.3340	374.905	441.122	0.445	352.337	
RADIAL POSITION		DIFFUSION FACTOR	ST. PRESS RISE COEFF	JH1	INLET ABS TANG. VEL	EXIT ABS TANG. VEL	INLET REL TANG. VEL	EXIT REL TANG. VEL	AXIAL VFL. RATIO
1	0.403	0.34825	0.3903	0.	240.732	666.886	418.155	418.155	1.049
2	0.410	0.41630	0.4369	0.	239.751	603.650	364.244	364.244	1.004
3	0.491	0.46612	0.4655	0.	277.357	543.166	272.475	272.475	1.198
4	0.444	0.50948	0.4683	0.	293.483	477.128	201.457	201.457	1.543
5	0.384	0.47639	0.3390	0.	344.337	401.974	96.785	96.785	
RADIAL POSITION		POLYTROPIC EFFICIENCY	TOT. PRESS RATIO	TCT. TEMP RATIO	FIXED INSTRUMENTATION		PRESSURE RATIO	Abs. EXIT FLOW ANG.	Abs. EXIT FLOW ANG.
1	0.7823	0.7868	1.157	1.055	0.	0.	1.1640	38.028	38.028
2	0.9035	0.9055	1.155	1.047	0.	0.	0.9419	38.071	38.071
3	0.8439	0.8471	1.153	1.049	0.	0.	0.9431	43.748	43.748
4	0.9321	0.9336	1.165	1.048	0.	0.	0.9431	41.637	41.637
5	0.9624	0.9633	1.177	1.050	0.	0.	0.9431	44.342	44.342
RADIAL POSITION		TRAVERSE ADIABATIC EFF.	TRAVERSE POLYTROPIC EFF.	TRAVERSE POLYTROPIC EFF.	ADIABATIC EFF.		POLYTROPIC EFF.	NOZZLE WEIGHT FLOW	
1	0.8805	0.8805	0.8805	0.8805	0.	0.	0.	112.41	
2	0.980	0.980	0.980	0.980	0.	0.	0.	0.9411	
3	0.950	0.950	0.950	0.950	0.	0.	0.	0.9326	
4	-0.0020	1.0089	-0.0086	-0.0086	0.	0.	0.	1.052	
5	-0.0053	1.0174	-0.0237	-0.0237	0.	0.	0.	1.046	
PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION									
RADIAL POSITION		TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO		TOT. TEMP RATIO	TOT. TEMP RATIO	
1	0.0264	0.8219	0.1212	0.1212	1.157	1.160	1.046	1.046	
2	0.0086	0.9432	0.0397	0.0397	1.159	1.159	1.046	1.046	
3	0.0107	0.9400	0.0484	0.0484	1.170	1.170	1.045	1.045	
4	-0.0020	1.0089	-0.0086	-0.0086	1.178	1.178	1.047	1.047	
5	-0.0053	1.0174	-0.0237	-0.0237	1.178	1.178	1.047	1.047	

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (ROTOR 2E)

N.A.S.A. COMPRESSOR OUTPUT DATA										
BLADE ELEMENT PERFORMANCE RESULTS										
	POINT NUMBER	READING NUMBER	DATE	4/14/1967	INLET ABS VELCITY	INLET ABS MACH NO.	INLET ABS VELCITY	INLET ABS MACH NO.	INLET ABS VELCITY	
RADIAL POSITION	REL. INLET FLOW ANG. 1 60, 637 2 66, 624 3 64, 464 4 61, 946 5 61, 994	INCID ANG MN.CMR.IN 10, 737 11, 164 12, 214 12, 236 11, 781	STRICT SURF 7, 677 6, 724 6, 504 5, 666 4, 118	INLET REL MACH NO. 0, 6392 0, 5923 0, 5428 0, 4897 0, 4170	ROTOR SPD AT INLET 666, 781 658, 213 603, 048 543, 638 463, 958	INLET ABS VELCITY	248, 243 261, 186 261, 016 260, 424 231, 069	INLET ABS MACH NO.	0, 223 0, 235 0, 235 0, 234 0, 208	
RADIAL POSITION	REL. EXIT FLOW ANG. 1 55, 119 2 49, 422 3 44, 172 4 31, 171 5 24, 590	REL. TURN ANG. T.E. 5, 709 4, 692 3, 009 2, 721 2, 810	EXIT REL. MACH NO. 0, 3853 0, 3863 0, 3042 0, 3153 0, 3118	ROTOR SPD AT EXIT 659, 458 439, 729 438, 075 344, 796 355, 782	EXIT ABS VELCITY	390, 748 393, 814 550, 309 495, 370 350, 585	EXIT ABS VELCITY	0, 342 0, 347 0, 350 0, 387 0, 437	EXIT ABS MACH NO.	0, 342 0, 347 0, 350 0, 387 0, 437
RADIAL POSITION	INFLUSSION FACTOR 1 0, 535 2 0, 473 3 0, 545 4 0, 503 5 0, 432	ST. PRESS RISE COEFF 0, 35289 0, 42476 0, 47432 0, 53497 0, 51153	INLET ABS TANG. VEL. 0, 3950 0, 4447 0, 4721 0, 4908 0, 3756	EXIT ABS TANG. VEL. 298, 887 271, 799 310, 189 312, 227 355, 448	INLET REL. TANG. VEL.	666, 781 604, 174 543, 638 477, 543 491, 780	INLET REL. TANG. VEL.	360, 571 352, 720 240, 120 161, 143 402, 323	INLET REL. TANG. VEL.	1, 015 1, 091 1, 051 1, 190 1, 545
RADIAL POSITION	POLYTROPIC EFFICIENCY 1 0, 6770 2 0, 8126 3 0, 7814 4 0, 8818 5 0, 9438	TOT. PRESS RATIO 0, 6839 0, 8167 0, 7959 0, 8845 0, 9451	TOT. TEMP RATIO 1, 155 1, 165 1, 158 1, 160 1, 180	INLET ABS VELCITY	666, 781 604, 174 543, 638 477, 543 491, 780	INLET ABS VELCITY	360, 571 352, 720 240, 120 161, 143 402, 323	INLET REL. TANG. VEL.	1, 015 1, 091 1, 051 1, 190 1, 545	
RADIAL POSITION	ADIABATIC EFFICIENCY 1 0, 6770 2 0, 8126 3 0, 7814 4 0, 8818 5 0, 9438	INLET ABS VELCITY	666, 781 604, 174 543, 638 477, 543 491, 780	INLET ABS VELCITY	666, 781 604, 174 543, 638 477, 543 491, 780	INLET ABS VELCITY	360, 571 352, 720 240, 120 161, 143 402, 323	INLET REL. TANG. VEL.	1, 015 1, 091 1, 051 1, 190 1, 545	
TRANSVERSE PRESSURE RATIO	= 1, 1673	FIXED INSTRUMENTATION							= 1, 1720	
TRANSVERSE ADIABATIC EFF.	= 0, 8993	ADIABATIC EFF.							= 0, 8882	
TRANSVERSE POLYTROPIC EFF.	= 0, 8134	POLYTROPIC EFF.							= 0, 8900	
FLOW COEFFICIENT L.F.	= 0, 080	NOZZLE WEIGHT FLOW							= 1, 03, 05	
FLOW COEFFICIENT T.F.	= 0, 050	WEIGHT FLOW							= 0, 93559	
PERCENT DESIGN SPEED = 50		T.E. CHECK WEIGHT FLOW/NZ.								
		T.C. CHECK WEIGHT FLOW/NZ.								
		WEIGHT FLOW								
RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO					TOT. TEMP RATIO	
1 0, 0455 2 0, 0210 3 0, 0223 4 0, 0088 5 -0, 0013	0, 7369 0, 8813 0, 8887 0, 9648 1, 0038	0, 2170 0, 0965 0, 1024 0, 0379 -0, 0057	1, 168 1, 170 1, 165 1, 173 1, 183	1, 062 1, 052 1, 050 1, 048 1, 049						

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

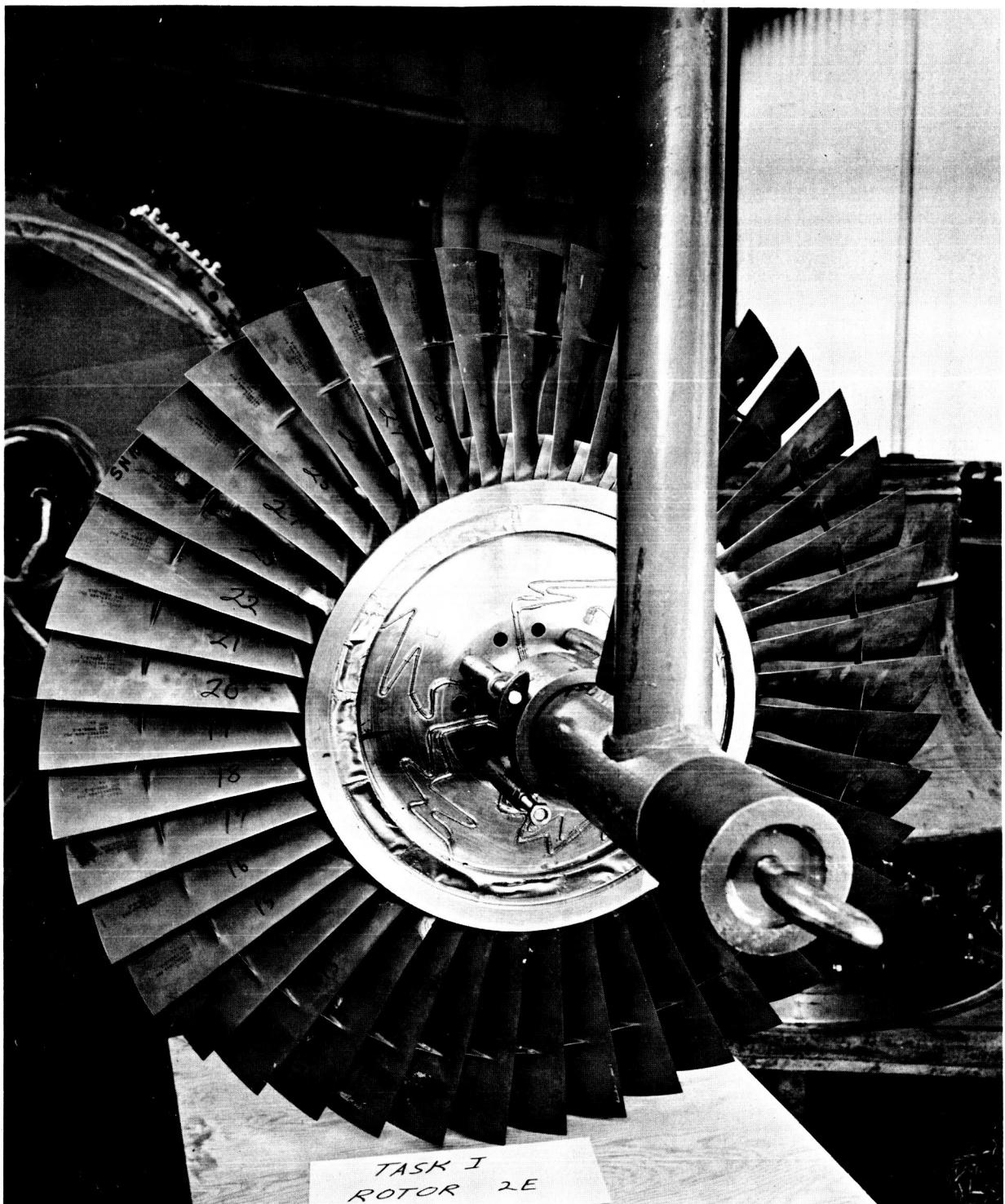


Figure 1(a). - Overall view of Rotor 2E.

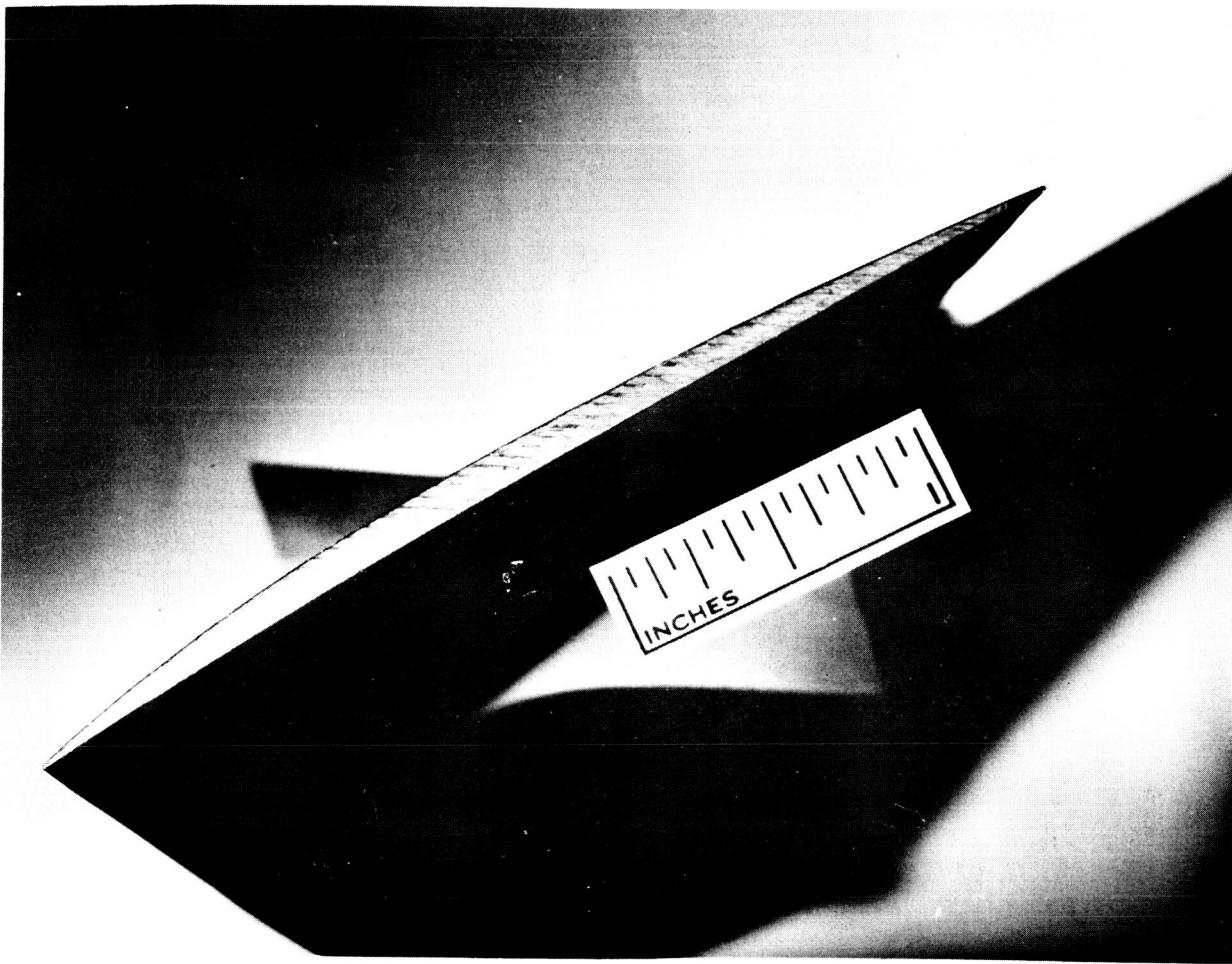


Figure 1(b). - Close-up view of tip section.

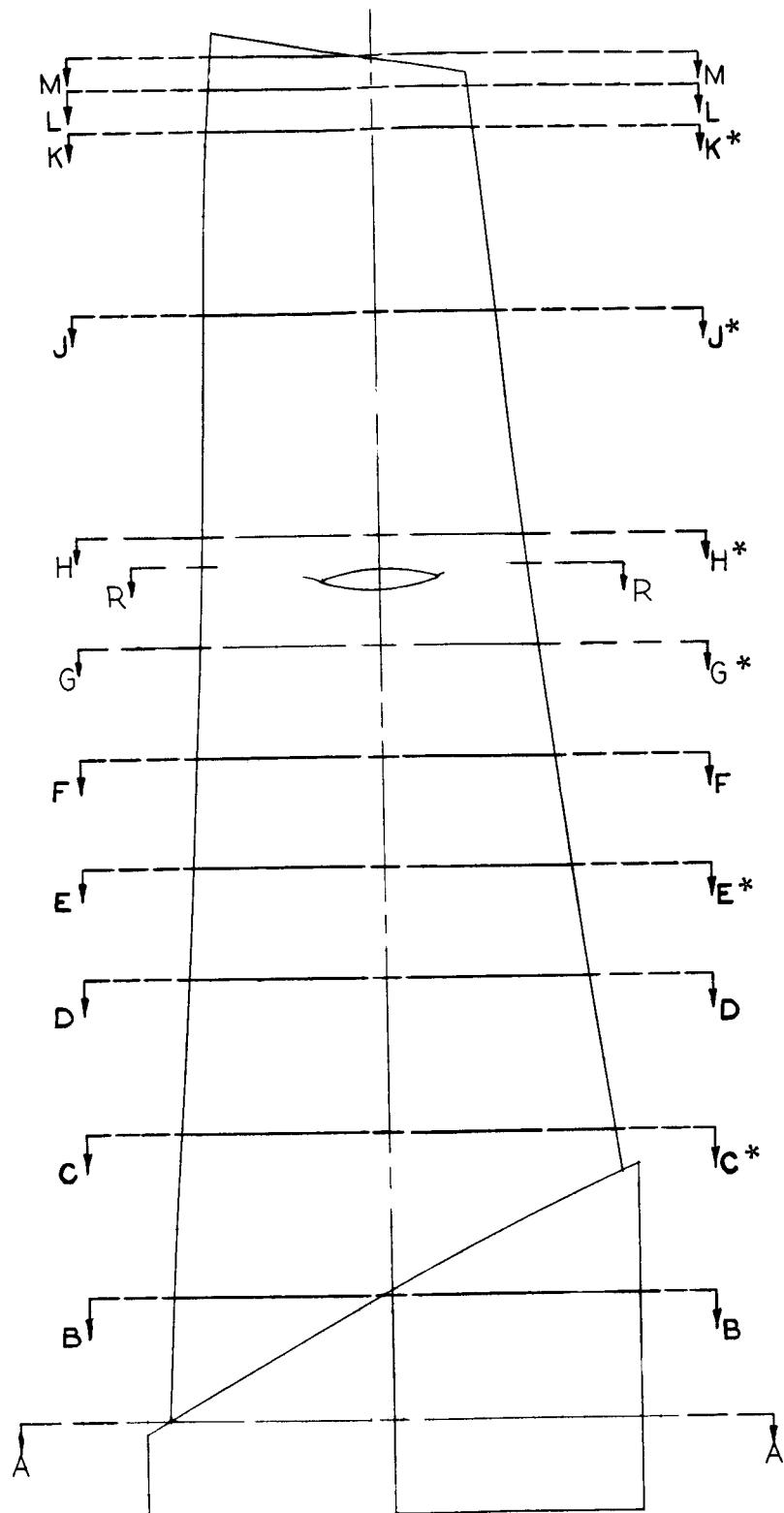


Figure 2. - Meridional view of rotor. Probograph inspection sections are indicated by asterisks.

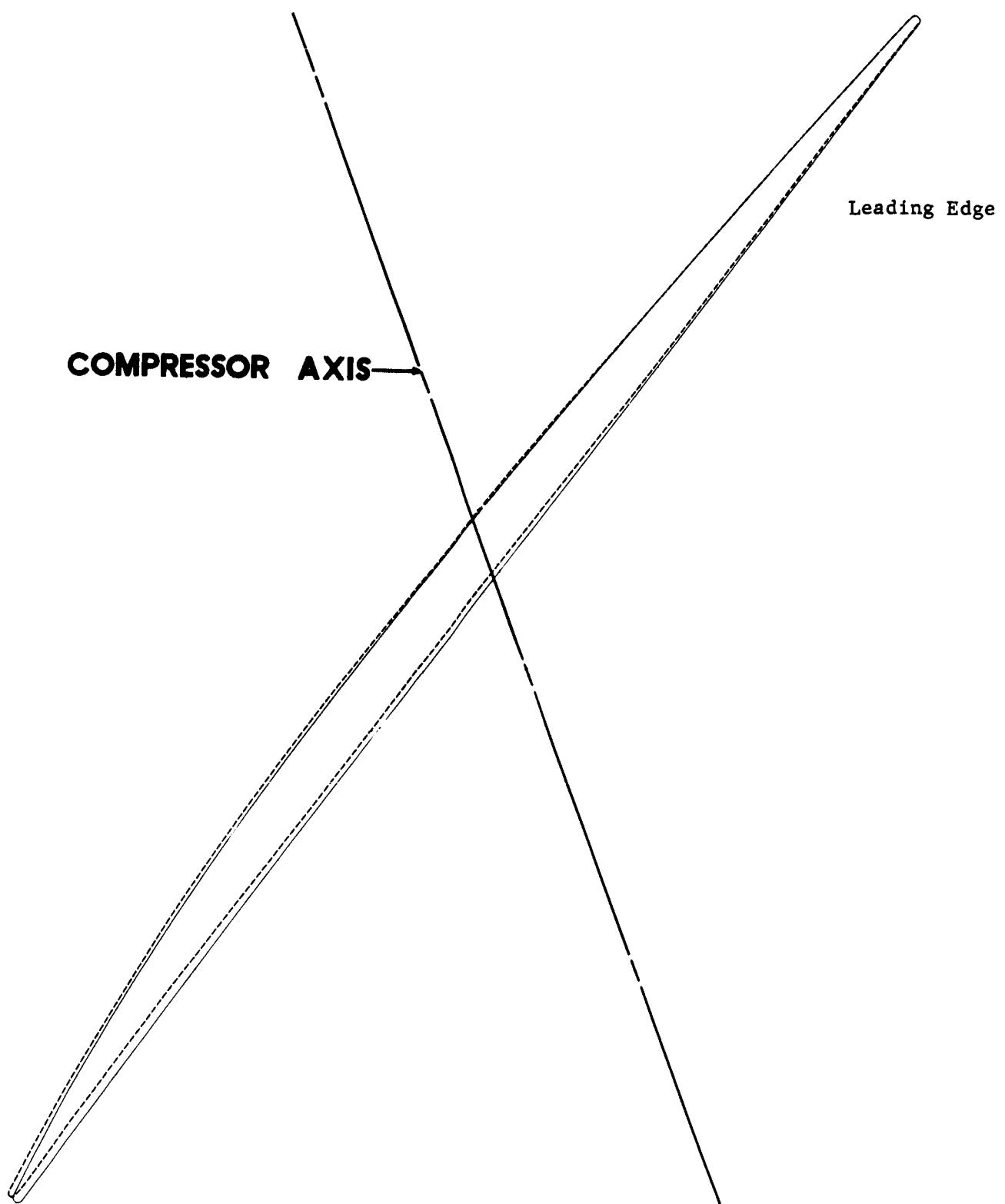


Figure 3(a). - Cylindrical cut of blade at section KK. The solid line represents design intent and the dashed line represents the average of seven measured samples.

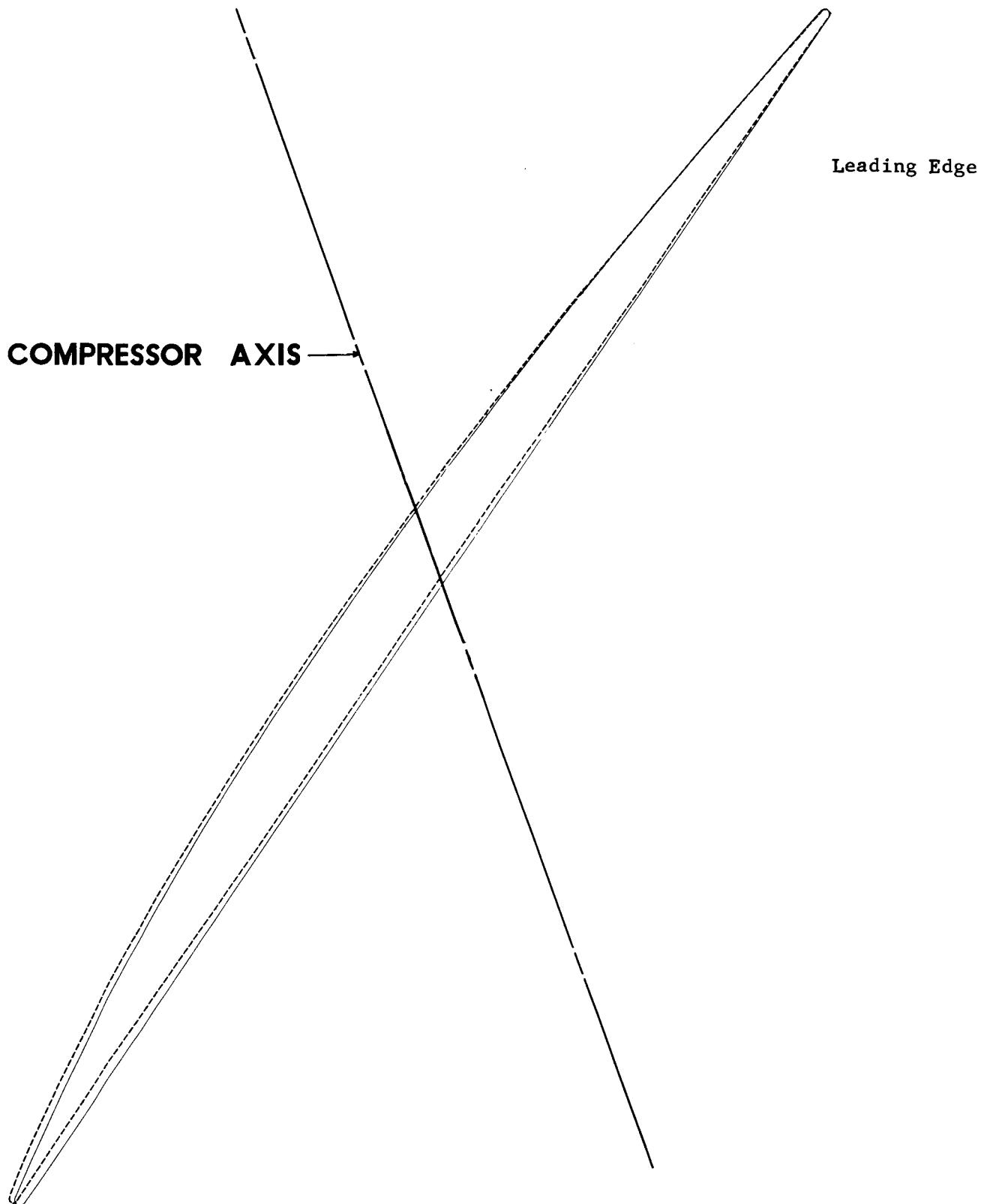


Figure 3(b). - Cylindrical cut of blade at section JJ. The solid line represents design intent and the dashed line represents the average of seven measured samples.

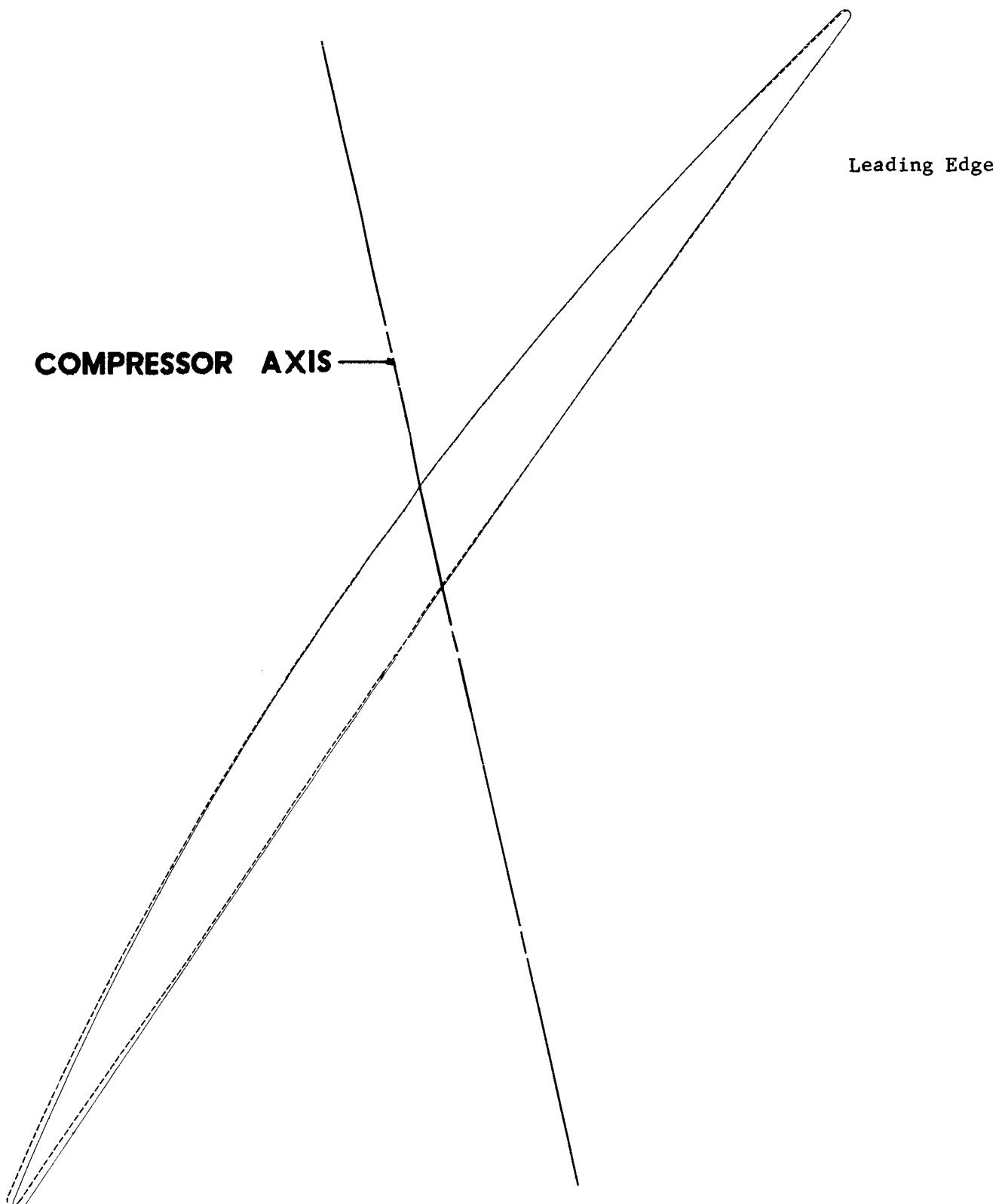


Figure 3(c). - Cylindrical cut of blade at section HH. The solid line represents design intent and the dashed line represents the average of seven measured samples.

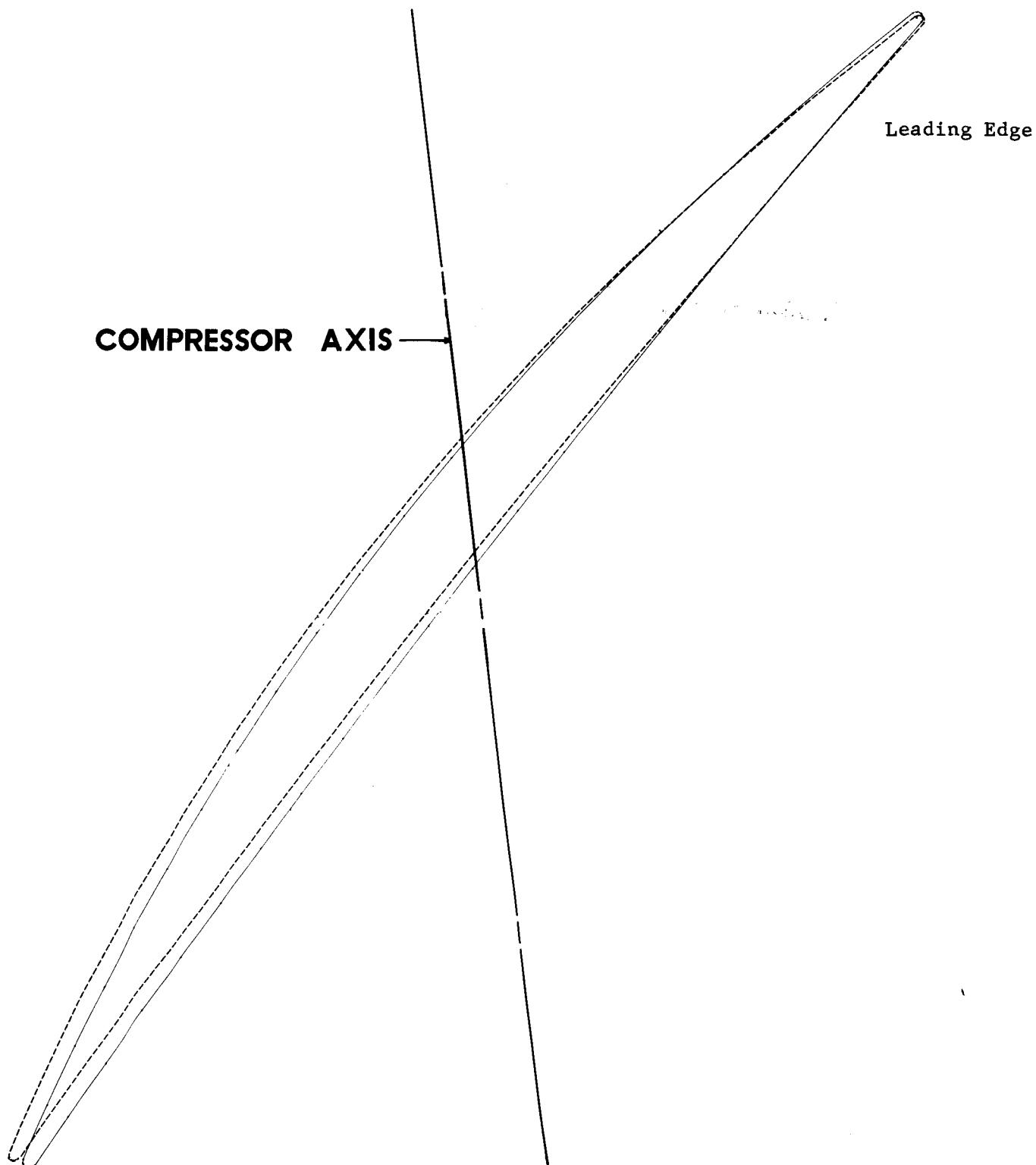


Figure 3(d). - Cylindrical cut of blade at section GG. The solid line represents design intent and the dashed line represents the average of seven measured samples.

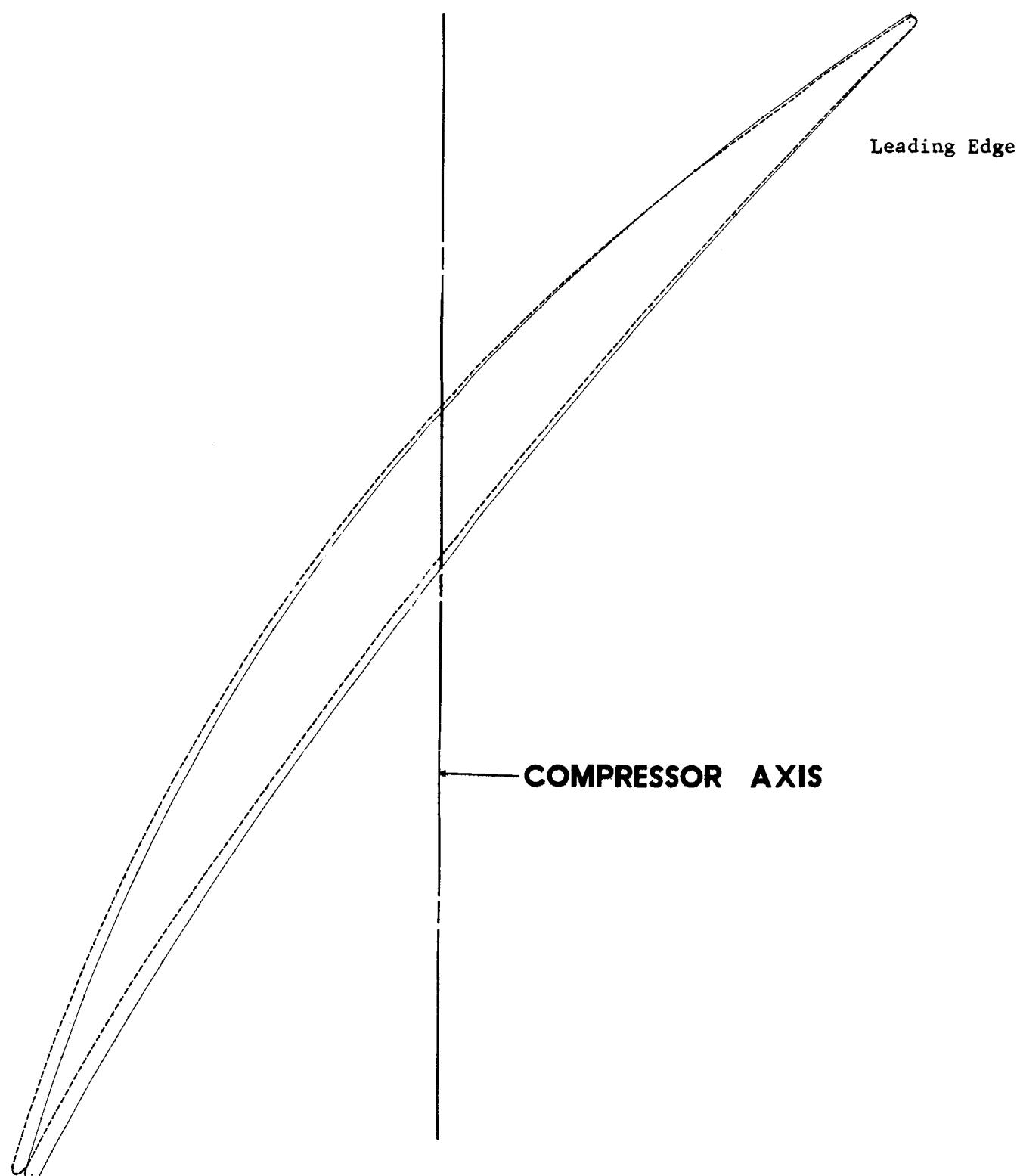


Figure 3(e). - Cylindrical cut of blade at section EE. The solid line represents design intent and the dashed line represents the average of seven measured samples.

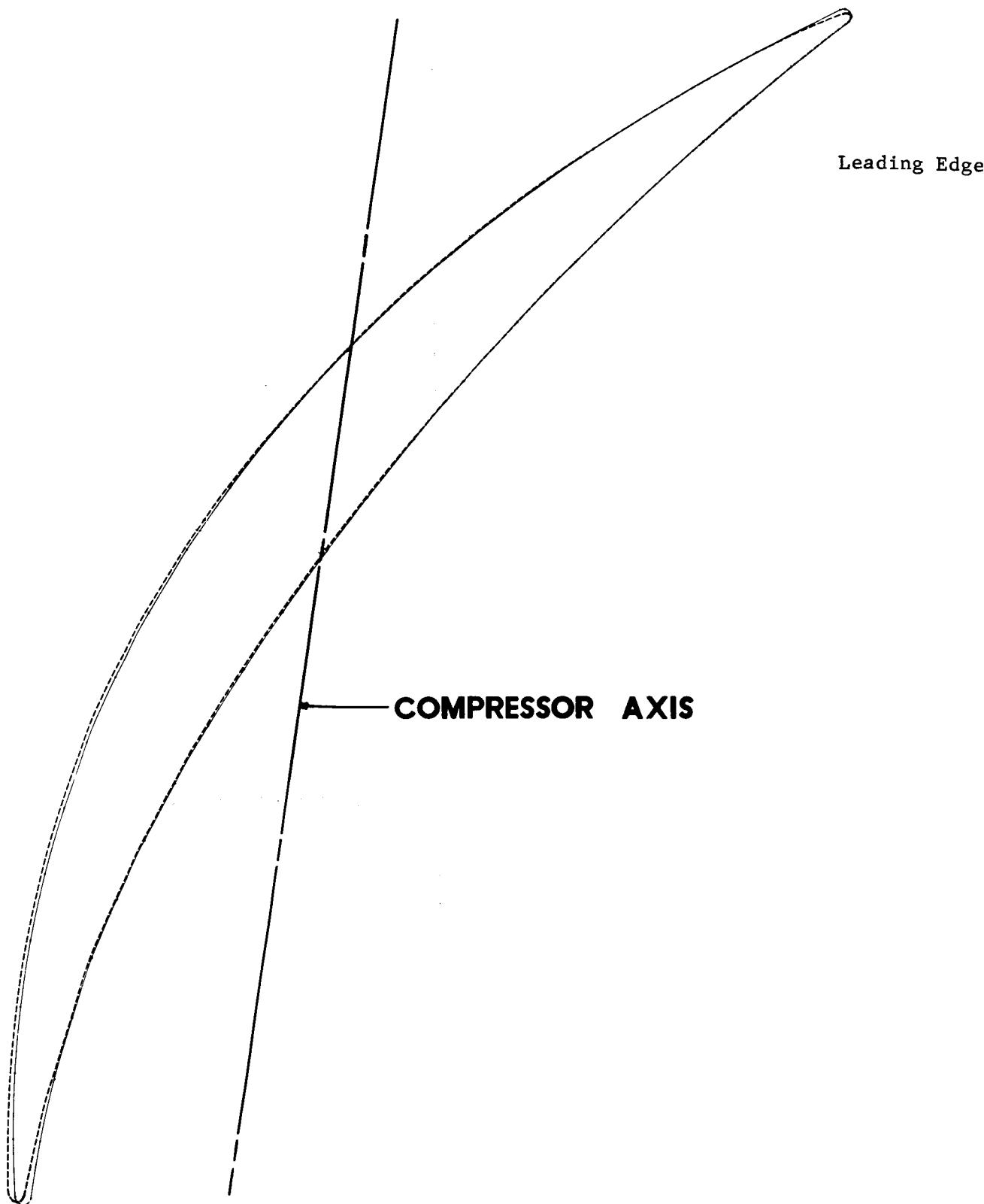


Figure 3(f). - Cylindrical cut of blade at section CC. The solid line represents design intent and the dashed line represents the average of seven measured samples.

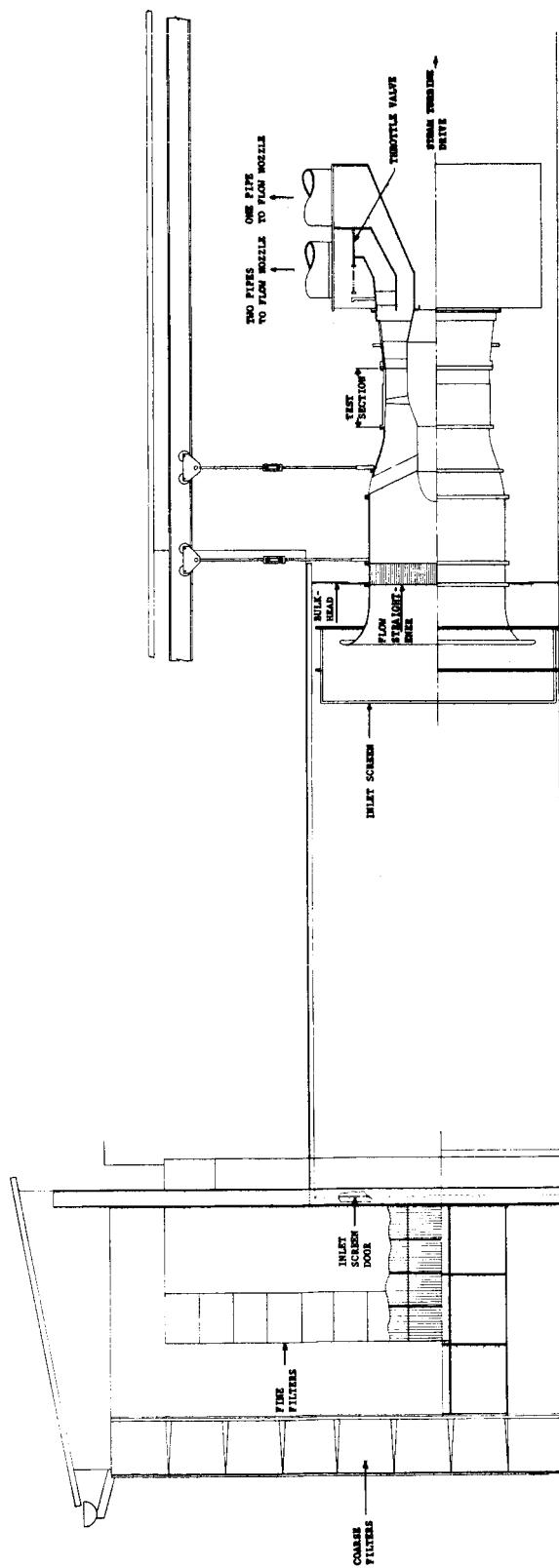


Figure 4. - House Compressor Test Facility.

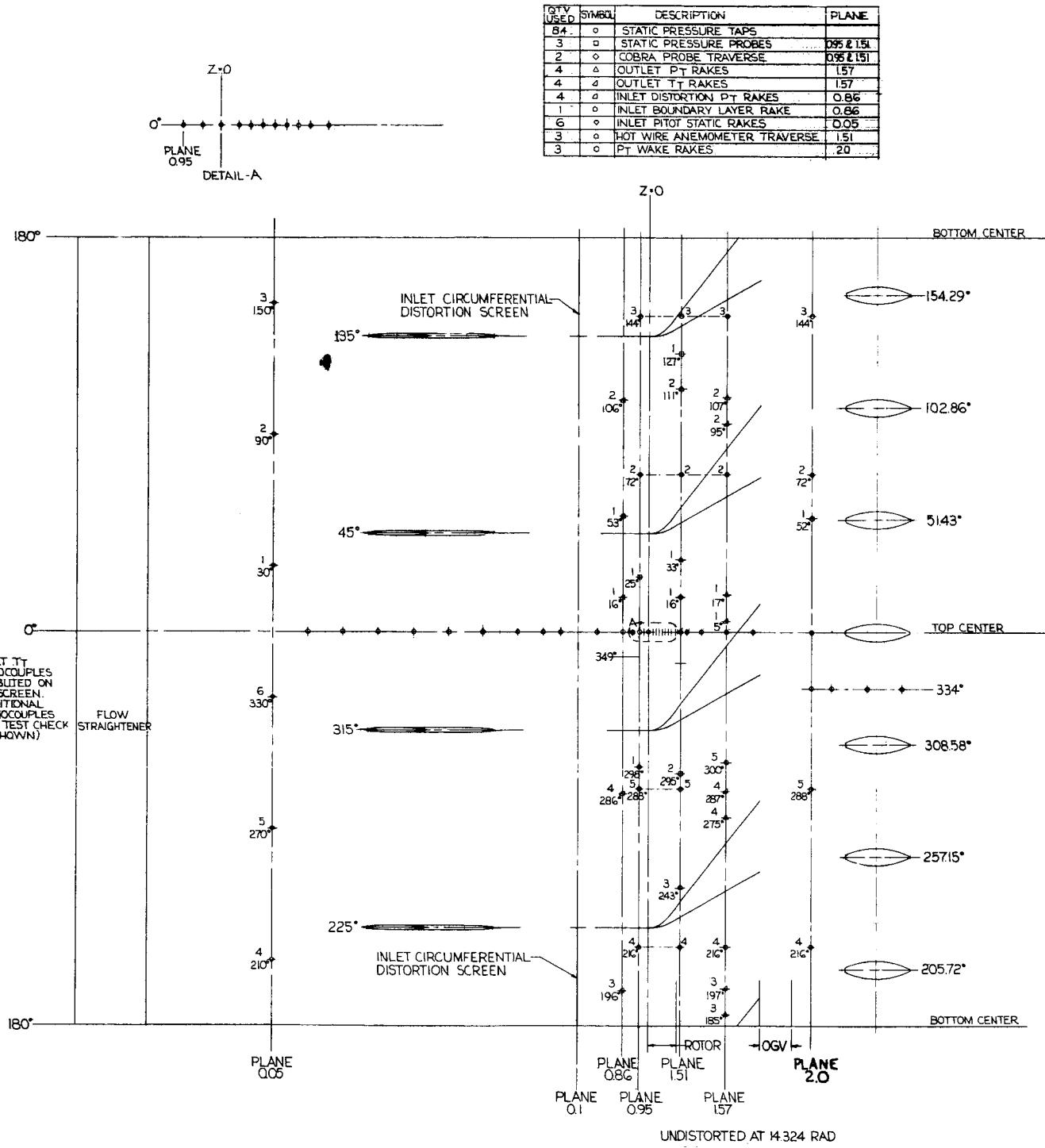
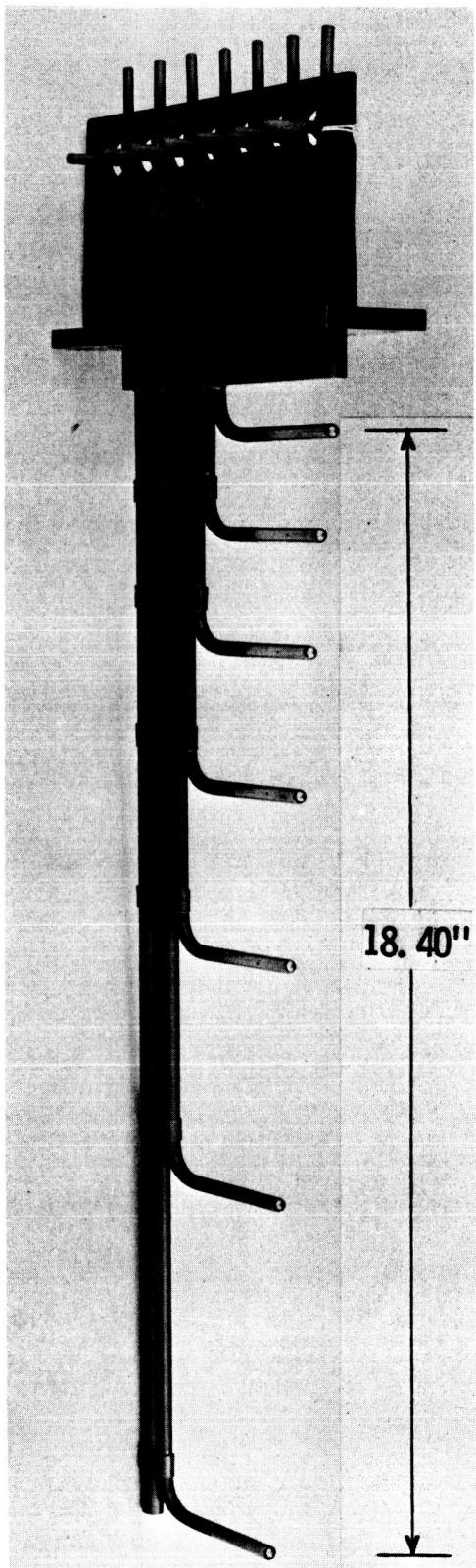
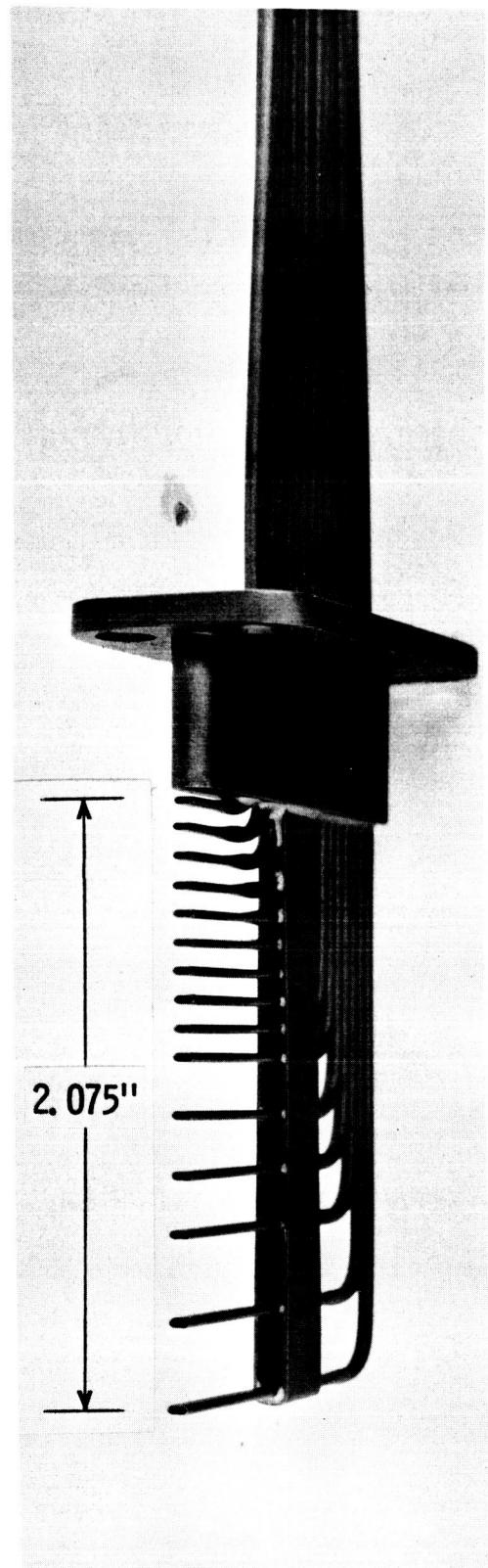


Figure 6. - Development showing circumferential location of instrumentation.

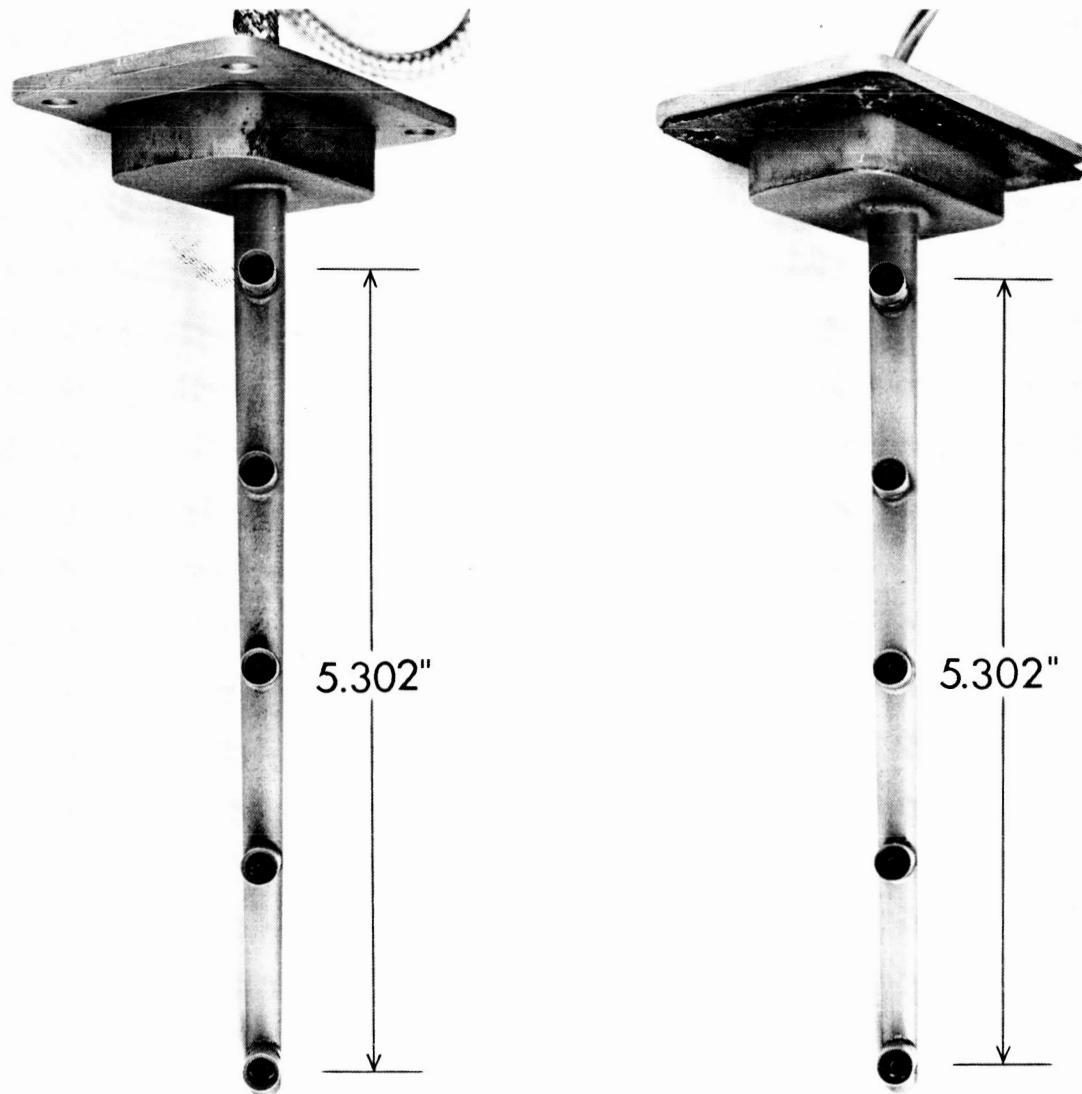


(a). - Inlet pitot-static rake.



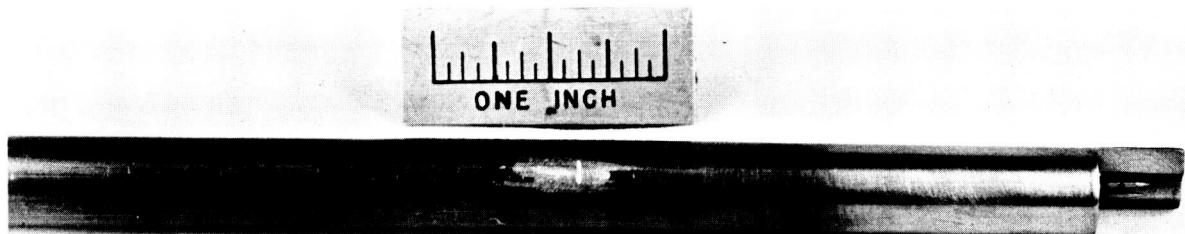
(b). - Casing boundary layer rake.

Figure 7. - Photographs of fixed instrumentation.

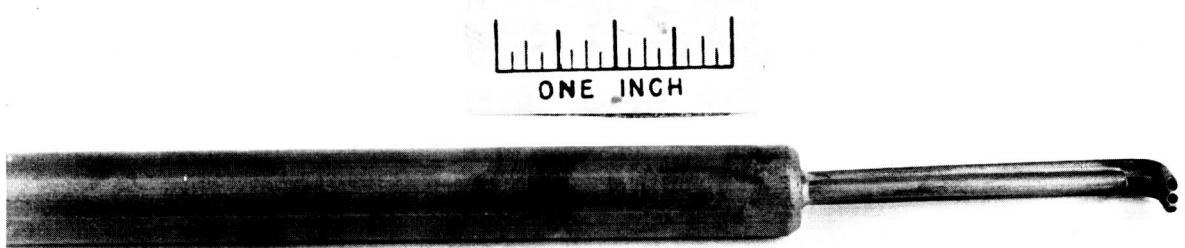


(c). Discharge total temperature rake. (d). Discharge total pressure rake.

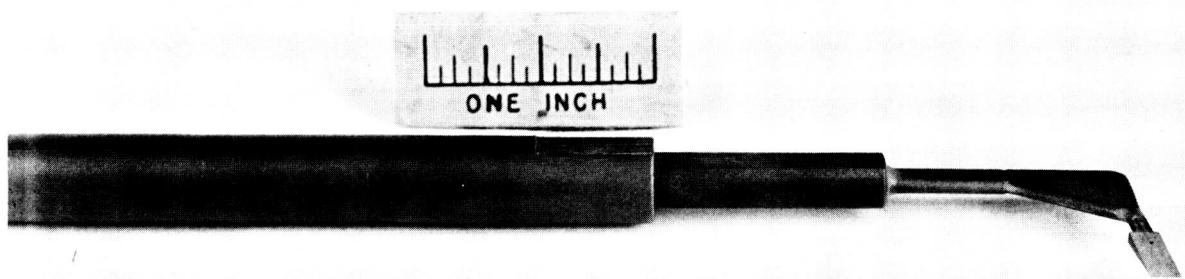
Figure 7. - Photographs of fixed instrumentation.



(a). - Shielded hot wire probe.



(b). - Cobra probe for sensing flow angle, total pressure
and total temperature.



(c). - Wedge probe for sensing static pressure.

Figure 8. - Photographs of traverse instrumentation.

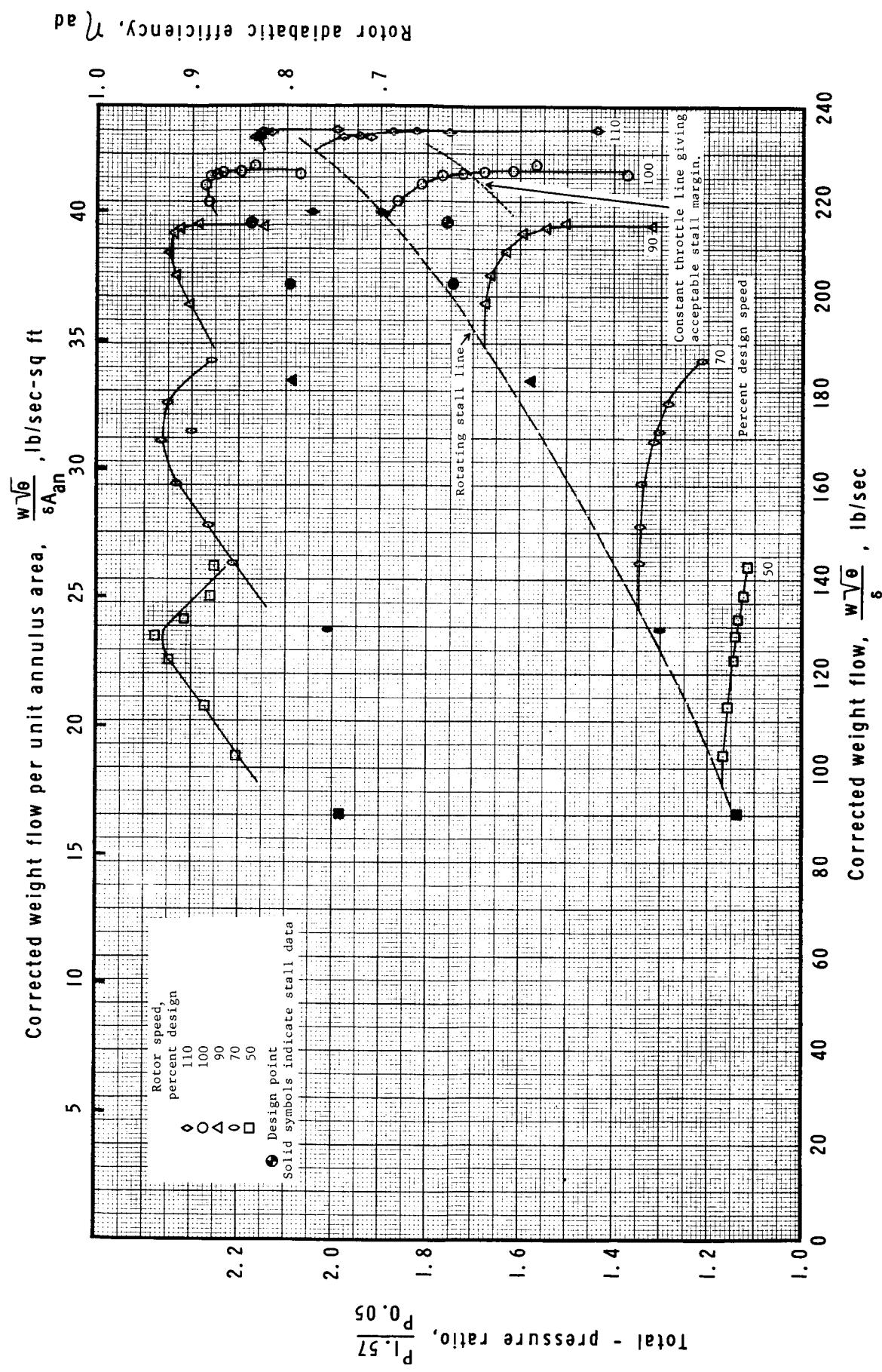
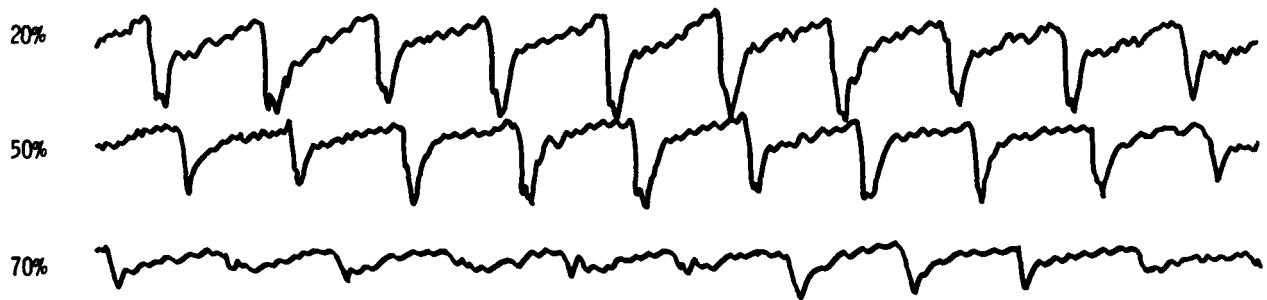


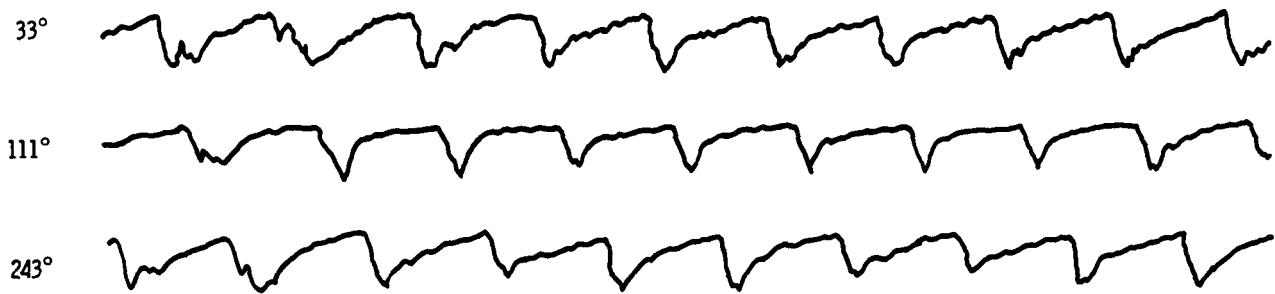
Figure 9. - Rotor performance map.

Immersion



(a) Sample of hot-wire anemometer traces at 90 percent design rotor speed.

Circumferential probe position



(b) Sample of hot-wire anemometer traces from 10 percent immersion at 90 percent design rotor speed.

Rotor speed, percent design	Number of stall cells	Stall cell speed Rotor speed	Radial extent of stall cell	Throttle setting at stall
50	3	.68	Full span	3.30
70	2	.64	Full span	4.90
90	1	.61	Full span	8.00
100	1	.66	Uncertain	9.25
110	1	.61	Uncertain	10.10

(c) Tabulation of stall data

Figure 10. - Sample hot-wire traces and tabulation of stall data.

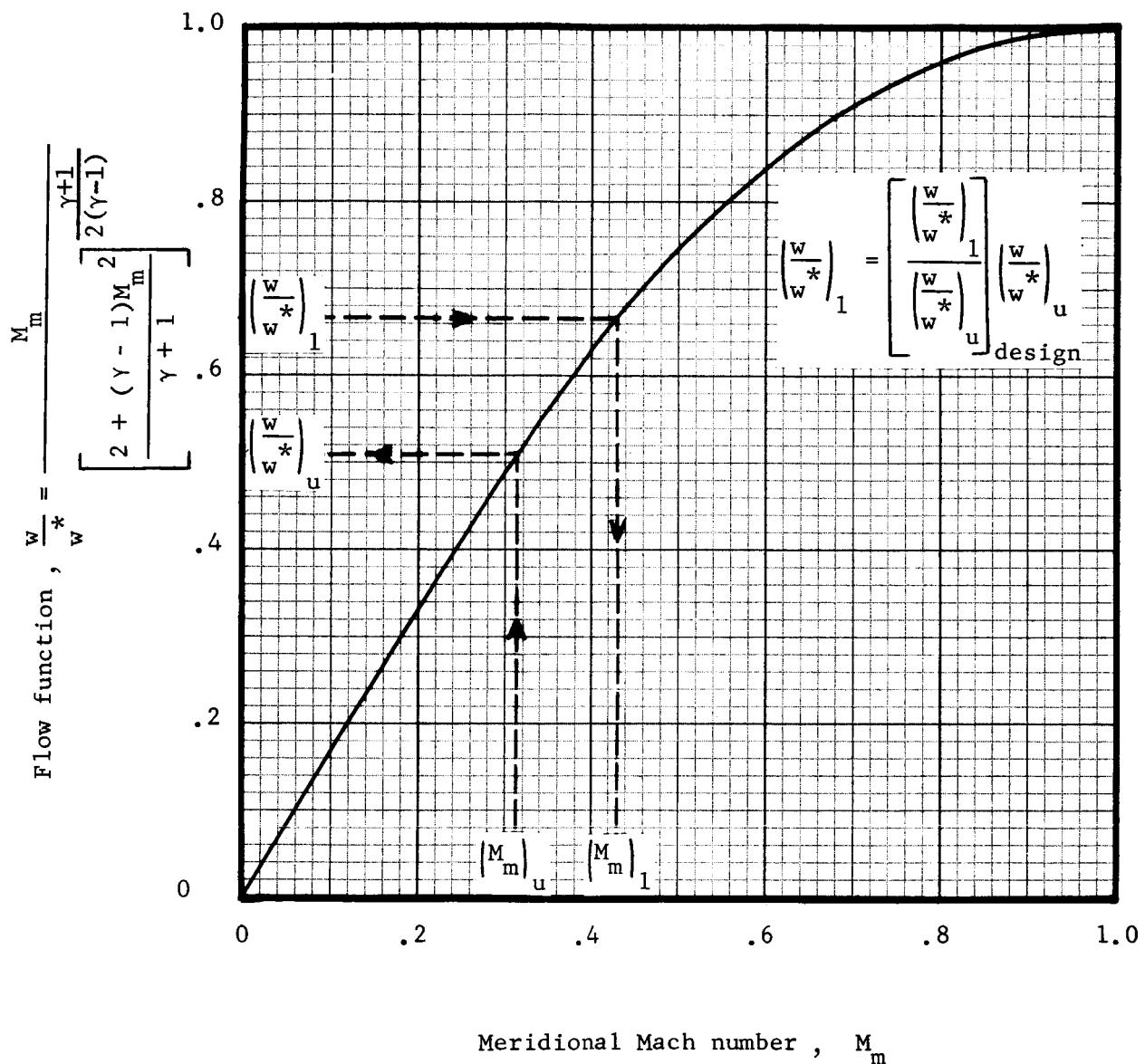


Figure 11. - Relationship between flow function and meridional Mach number - used for transferring traverse measurements to blade edges. Dashed lines with arrows and inset formulas indicate calculation sequence for sample case at leading edge.

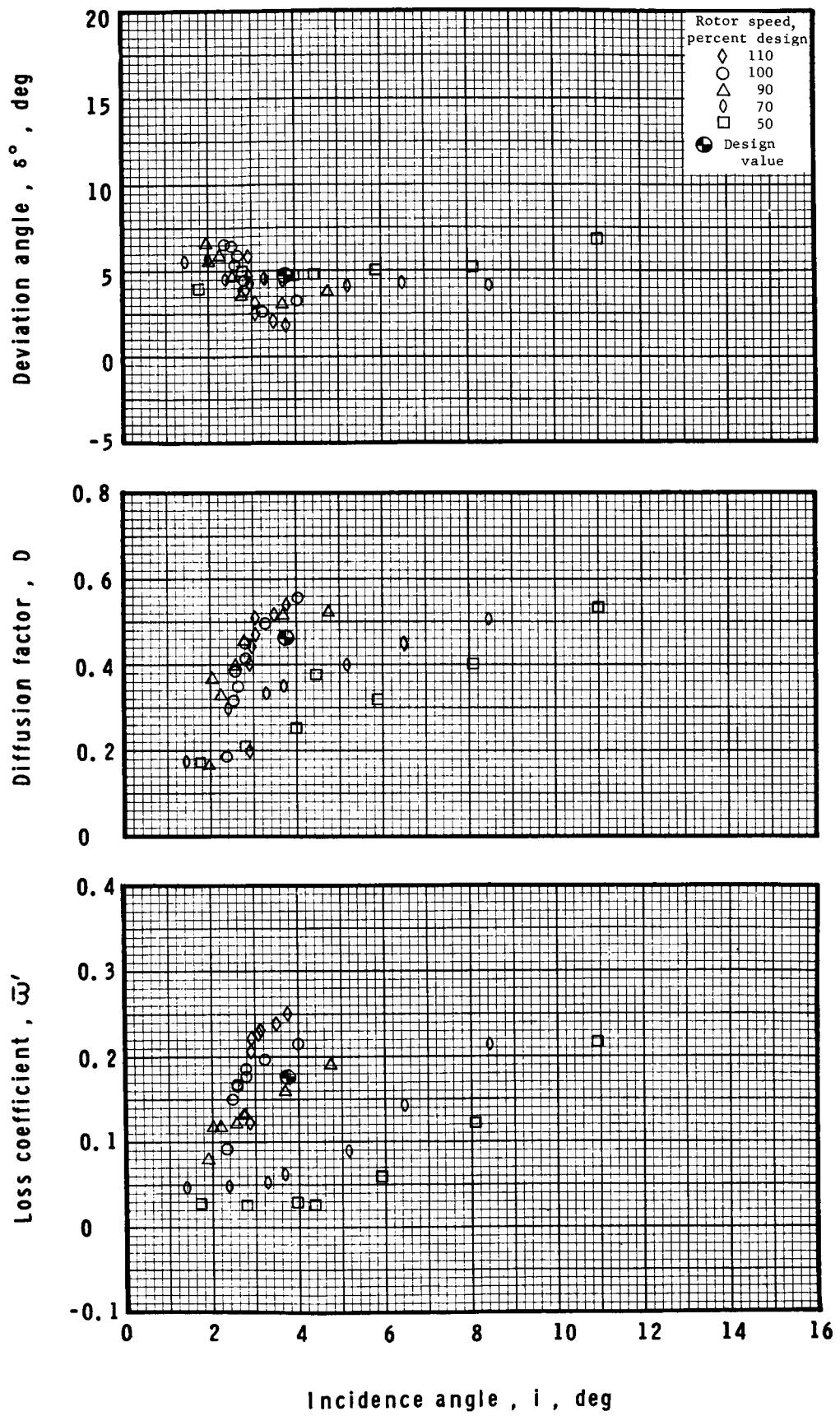


Figure 12(a). - Blade element data measured at 10% immersion from tip.

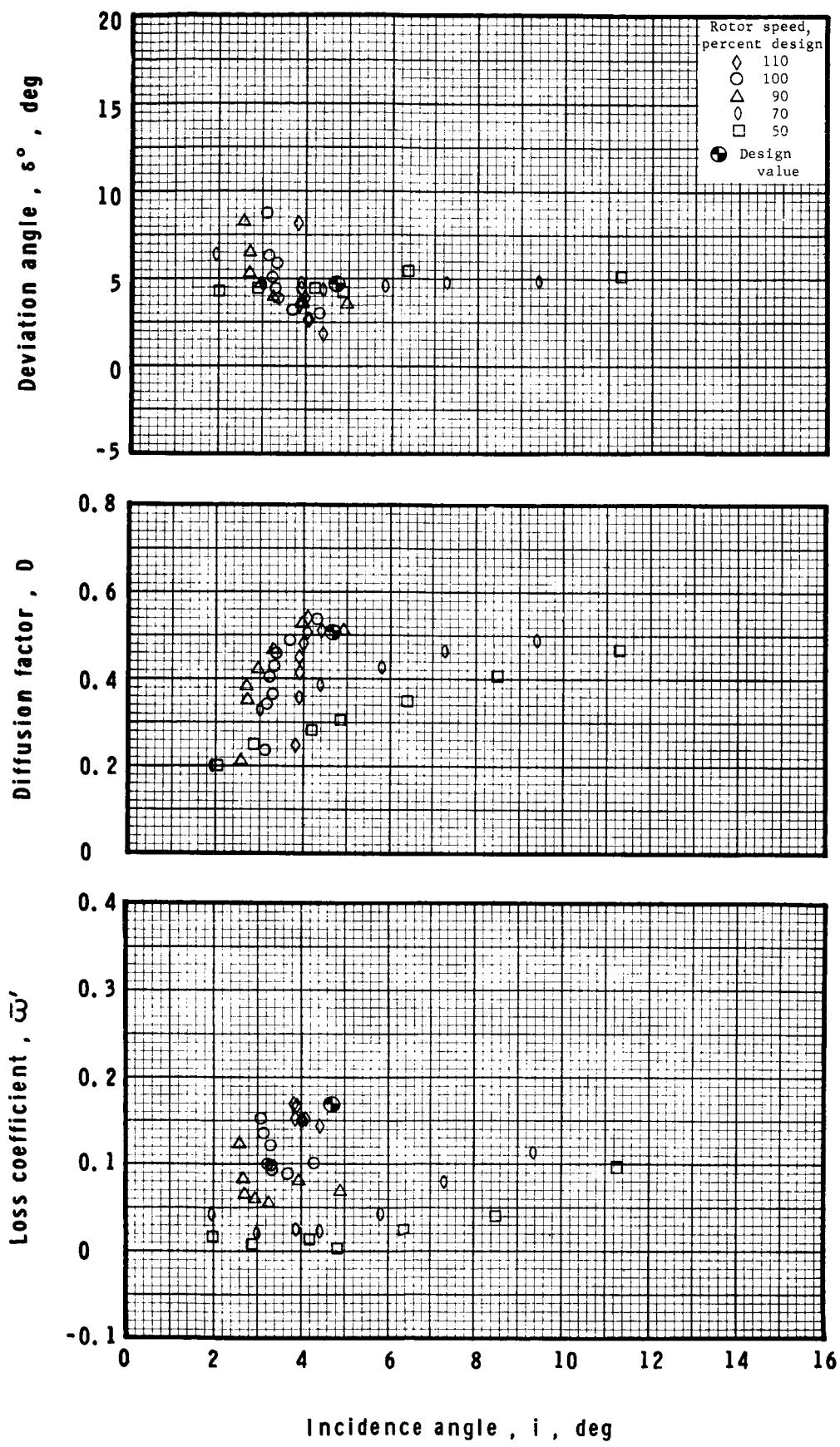


Figure 12(b). - Blade element data measured at 30% immersion from tip.

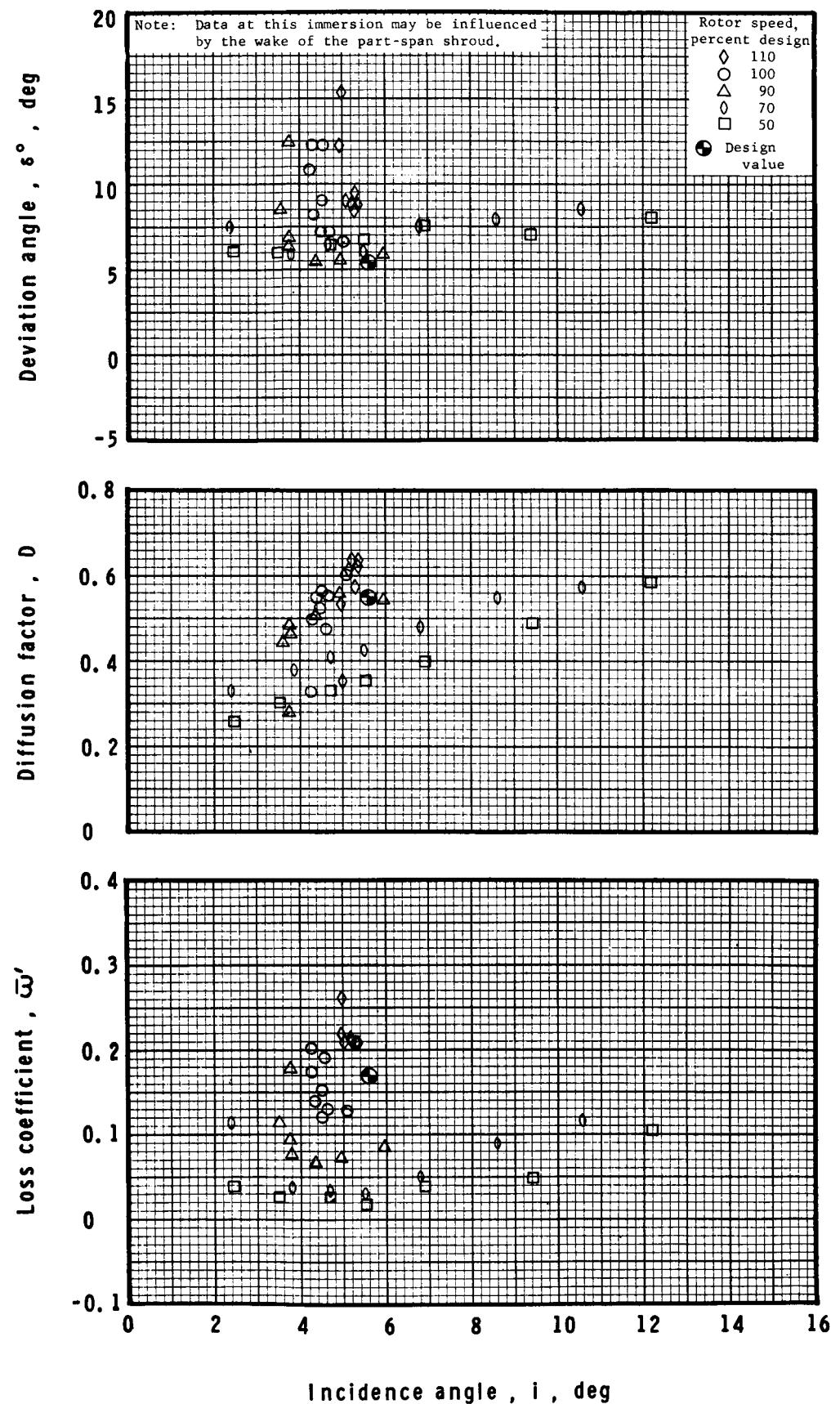


Figure 12(c). - Blade element data measured at 50% immersion from tip.

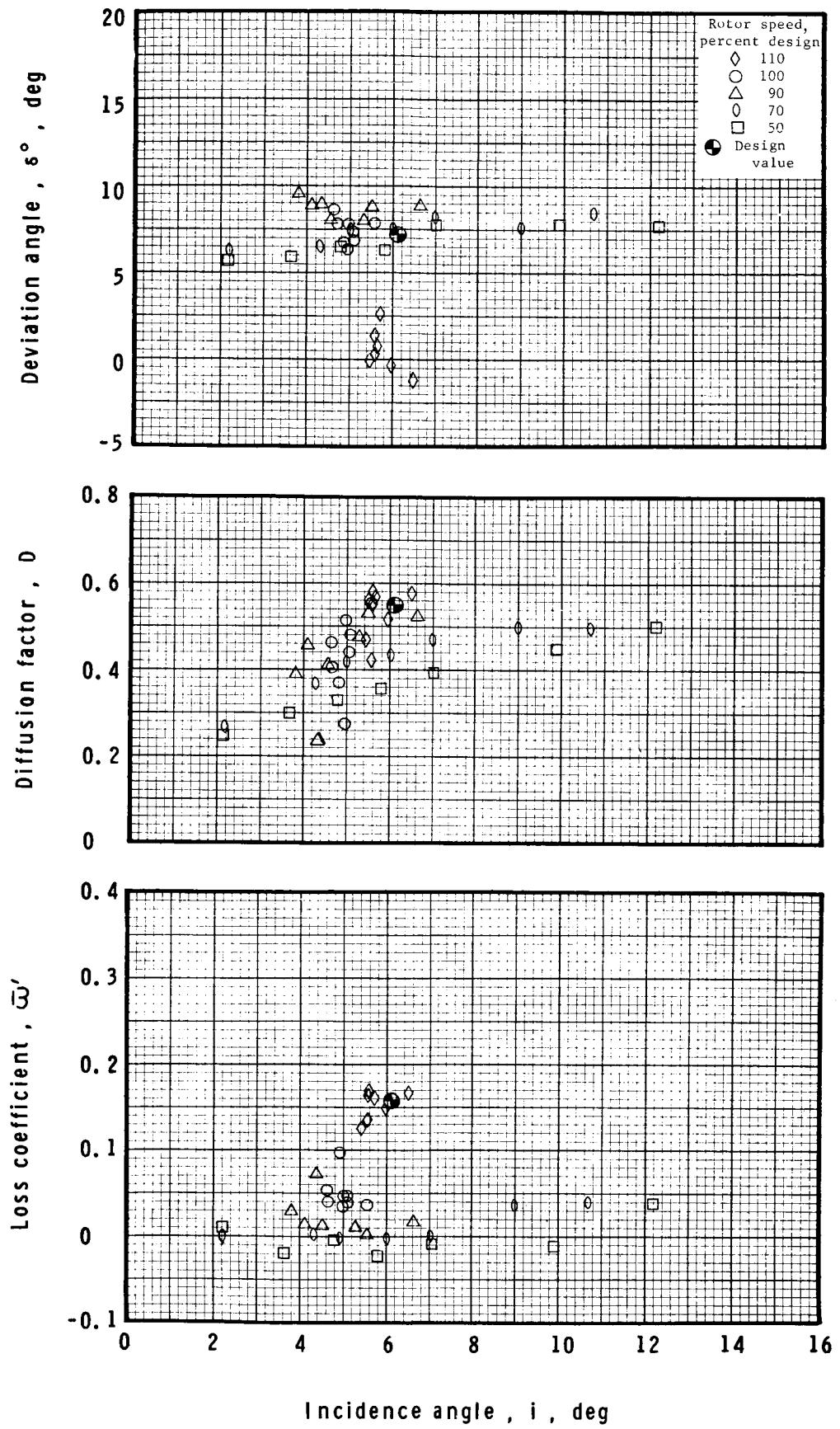


Figure 12(d). - Blade element data measured at 70% immersion from tip.

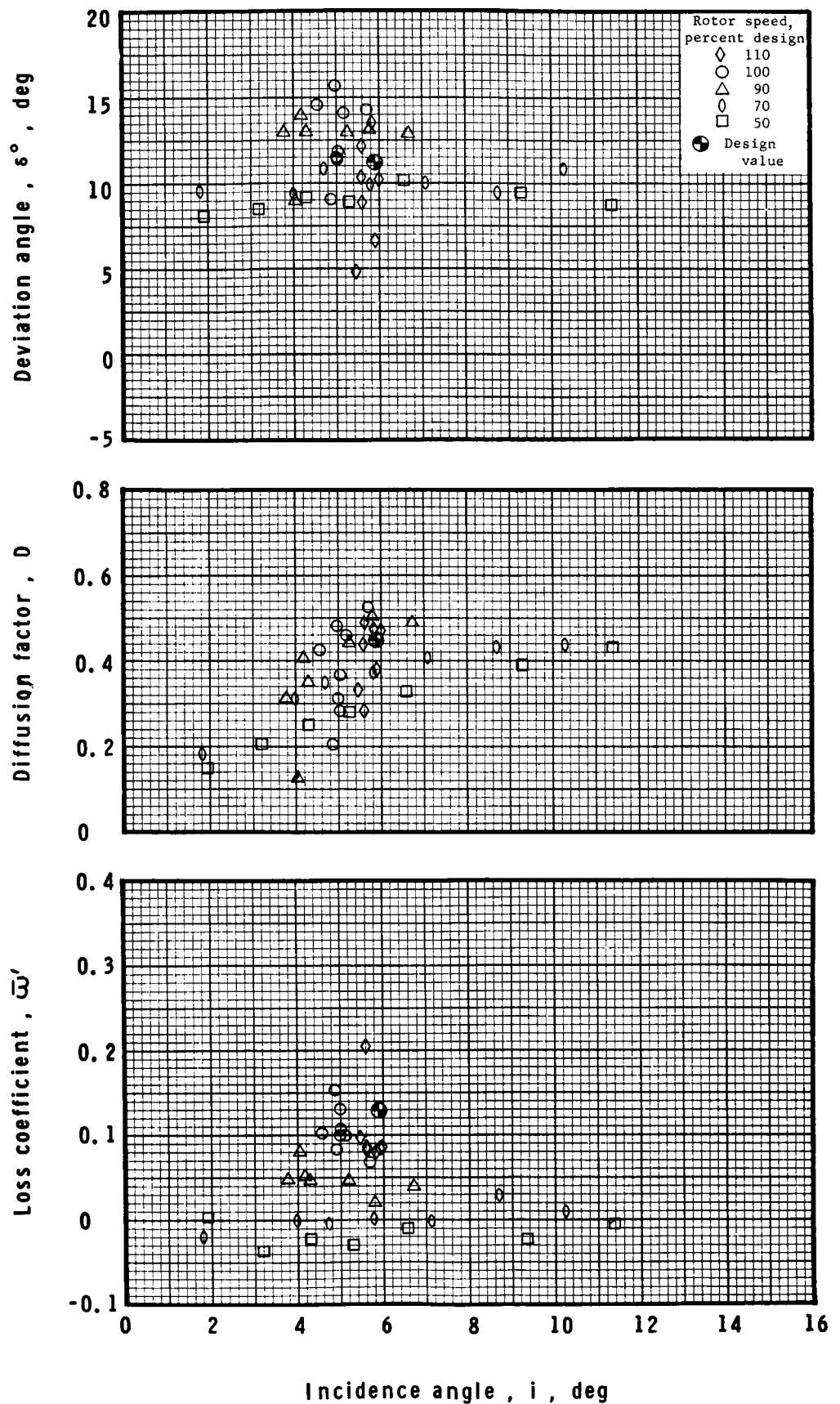


Figure 12(e). - Blade element data measured at 90% immersion from tip.

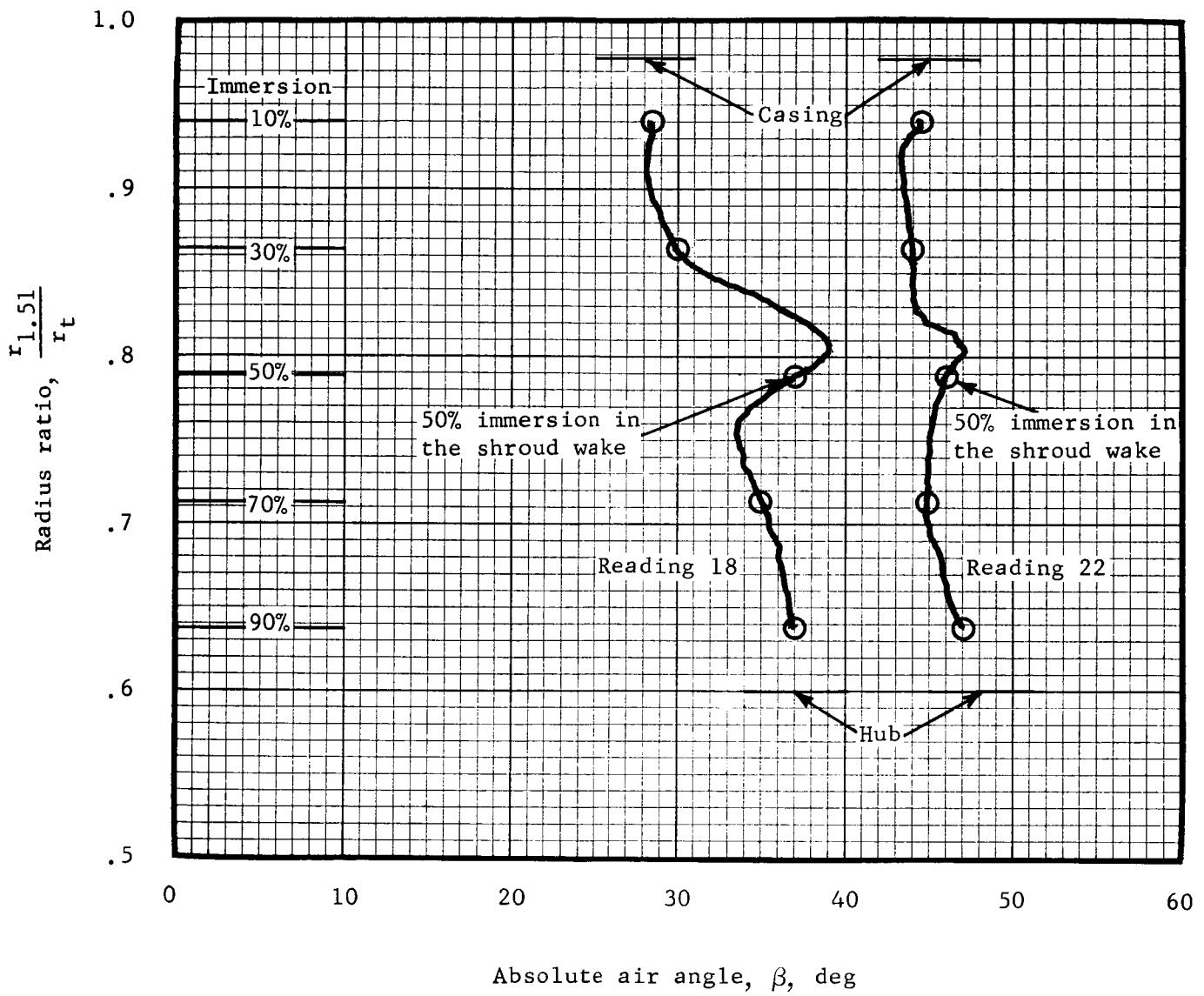


Figure 13. - Two rotor exit flow angle traverses at 90% speed. No radial movement of the part-span shroud wake is observed as the rotor is throttled.

2/2/74

REPORTS DISTRIBUTION LIST FOR
SINGLE STAGE EXPERIMENTAL EVALUATION OF
HIGH MACH NUMBER COMPRESSOR ROTOR BLADING

CONTRACT NAS3-7617

1.	NASA-Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135 Attention:	Report Control Office MS 5-5	1
		Technical Utilization Office MS 3-19	1
		Library MS 60-3	1
		Fluid System Component Division MS 5-3	1
		Pump & Compressor Branch MS 5-9	6
	I.I. Pinkel	MS 5-3	1
	A. Ginsburg	MS 5-3	1
	P. Hacker	MS 5-3	1
	M.J. Hartmann	MS 5-9	1
	W.A. Benser	MS 5-9	1
	D.M. Sandercock	MS 5-9	1
	L.J. Herris	MS 5-9	1
	C.L. Ball	MS 5-9	1
	J Howard Childs	MS 60-4	1
	Dr. W.H. Roudebush	MS 60-6	1
	J.H. Deford	MS 60-5	1
	S. Lieblein	MS 7-1	1
	Projects Branch	MS 60-6	16
	L. Macioce	MS 60-6	1